



Contribution to HiLiftPW-3

Marc Langlois

Hong Yang Kurt Sermeus

Advanced Aerodynamics
Bombardier

030

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Summary of cases completed: Solver: Dragon - TM: Wilcox k- ω 88

Case	Alpha=8, Fully turb, grid study	Alpha=16, Fully turb, grid study	Other
1a (full gap)	yes	yes	Full polar on all grid levels
1b (full gap w adaption)	no	no	
1c (partial seal)	no	no	
1d (partial seal w adaption)	no	no	
Other			

Grids: B2 (Pointwise)

Case	Polar, Fully turb	Polar, specified transition	Polar, w transition prediction	Other
2a (no nacelle)	yes	yes	no	
2b (no nacelle w adaption)	no	no	no	
2c (with nacelle)	no	no	no	
2d (with nacelle w adaption)	no	no	no	
Other				

Grids: E (ANSA)

Case	2D Verification study	Other
3	yes	
Other		

Grids: Supplied

Summary of cases completed: Solver: Dragon – TM: Wilcox k- ω 88

Case	Alpha=8, Fully turb, grid study	Alpha=16, Fully turb, grid study	Other
1a (full gap)	yes	yes	Full polar on all grid levels
1b (full gap w adaption)	no	no	
1c (partial seal)	yes	yes	Full polar on all grid levels
1d (partial seal w adaption)	no	no	
Other			

Grids: In-house (Pointwise)

Case	Polar, Fully turb	Polar, specified transition	Polar, w transition prediction	Other
2a (no nacelle)	yes	yes	no	
2b (no nacelle w adaption)	no	no	no	
2c (with nacelle)	yes	yes	no	
2d (with nacelle w adaption)	no	no	no	
Other				

Grids: In-house
(Pointwise)

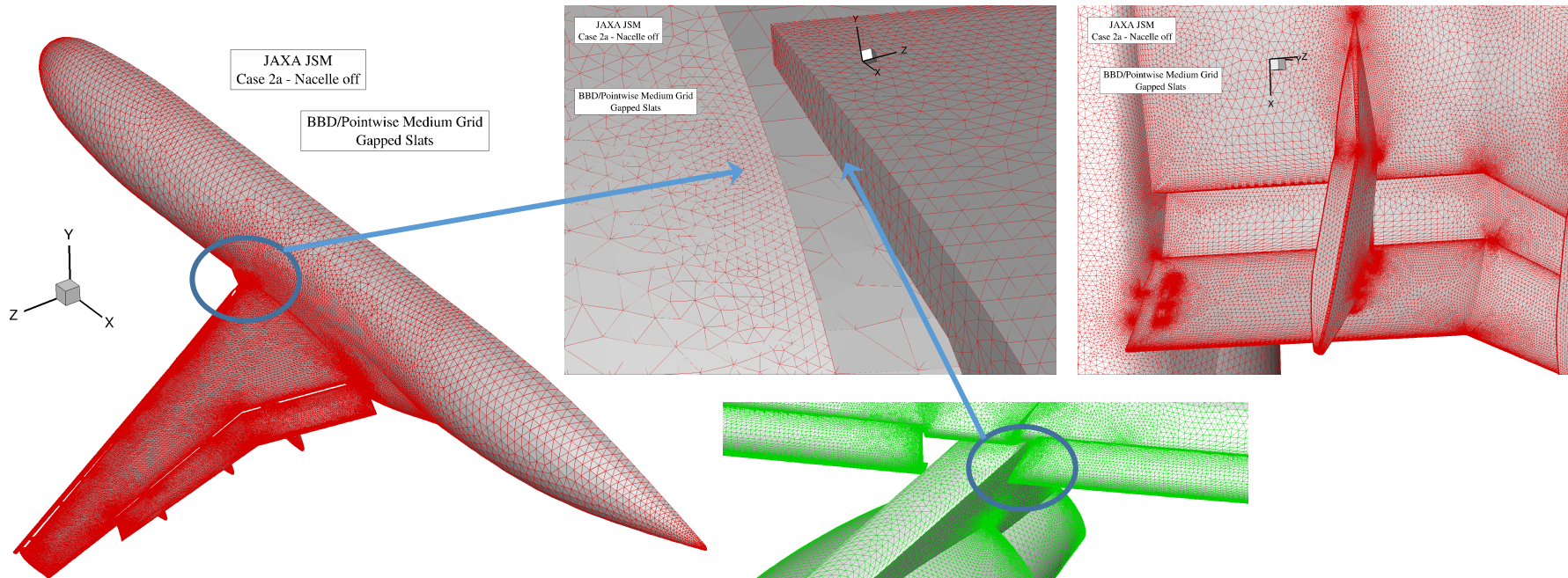
Brief overview of grid systems

Grid System	Case(s)	If committee grid, report any problems/issues If user grid, reason for generating grid system
Committee – NASA CRM - Grids B2 (Pointwise)	1a	Had to regenerate CGNS files from Pointwise Could not preprocess extra-fine grid
User – NASA CRM – Mixed-element unstructured (Pointwise)	1a, 1c	Initially had issues reading the supplied grids Want to use this exercise as validation for our whole CFD package
Committee – JAXA JSM – Grids B (Solar)	2a	Solver diverged
Committee – JAXA JSM – Grids C2 (VGrid mixed)	2a	Convergence issues at high AoAs
Committee – JAXA JSM – Grids D	2a	Had to edit CGNS file for bc's and components (applies to all committee grids)
User – JAXA JSM - Mixed-element unstructured (Pointwise)	2a, 2c	Initially had issues reading the supplied grids Want to use this exercise as validation for our whole CFD package

Dragon Flow Solver

- Bombardier in-house 3D hybrid structured-unstructured RANS solver
 - Cell-centered, coupled solver
- Implicit time integration with LU-SGS approach
 - 1st-order accurate in time for steady simulations
- 2nd-order accurate Roe's upwind scheme for convective flux and central differencing scheme for viscous flux discretization
- Many turbulence models implemented
 - Wilcox k- ω 1988 model with curvature extension used
- Parallel large-scale simulation capability with non-blocking MPI
- Interfaced with CGNS data produced by main-stream commercial grid generators
- Ref.: Yang, H. and Langlois, M. "Towards Accurate Simulation of Aircraft High-Lift Flows with One- and Two-Equations Turbulence Models", 62nd CASI Aeronautics Conference, May 2015.

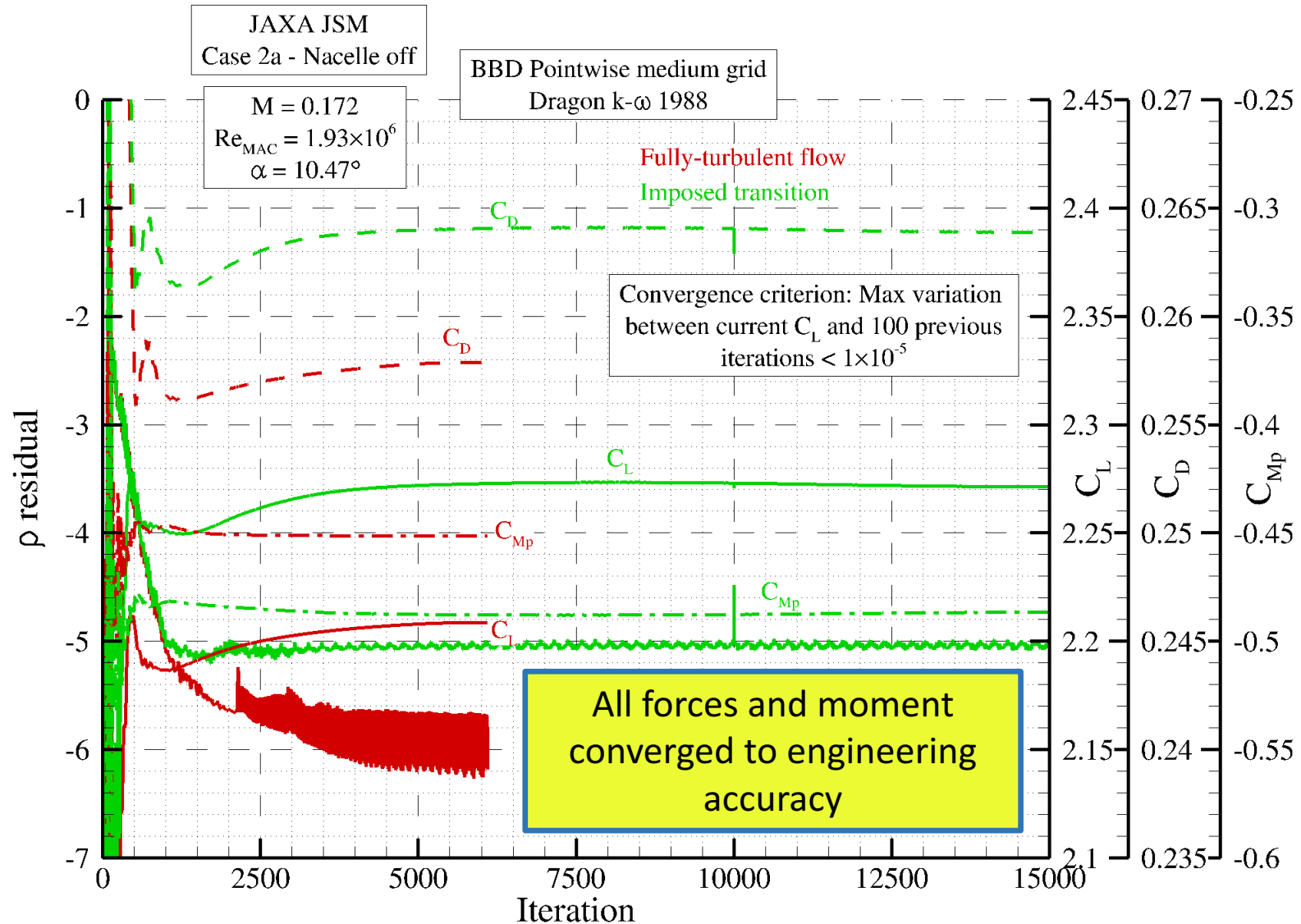
JAXA JSM results – Cases 2a/2c – Bombardier grids



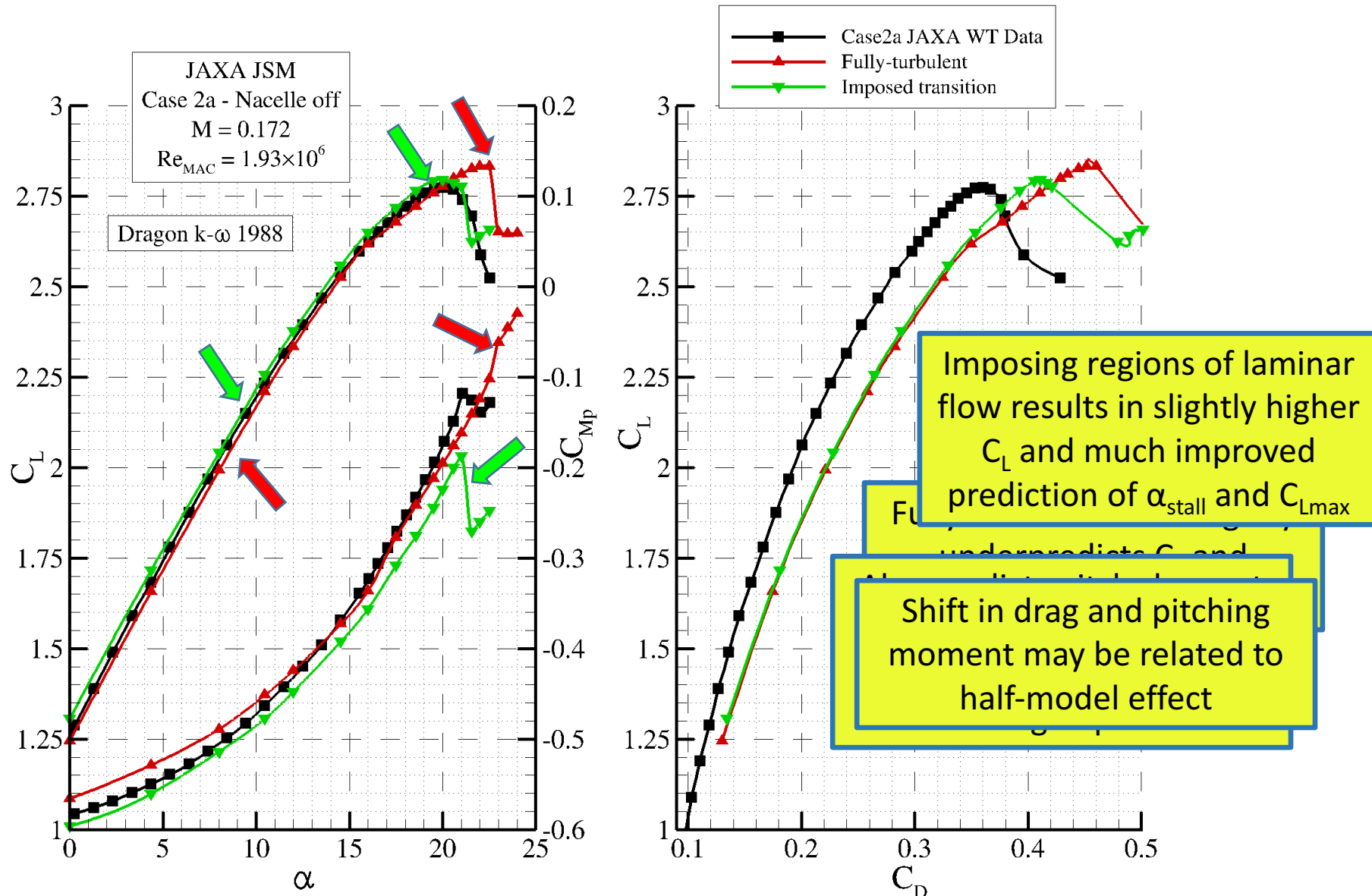
	Case 2a	Case 2c
Nodes	17 708 448	21 720 656
Cells	41 695 790	50 488 218
Fuselage	35 826	35 826
Wing	224 280	233 538
Slats	289 914	247 623
Flaps	253 048	253 048
Nacelle	-	174 472

Generated with Pointwise
Medium grid guidelines

JAXA JSM results – Transition influence: convergence history

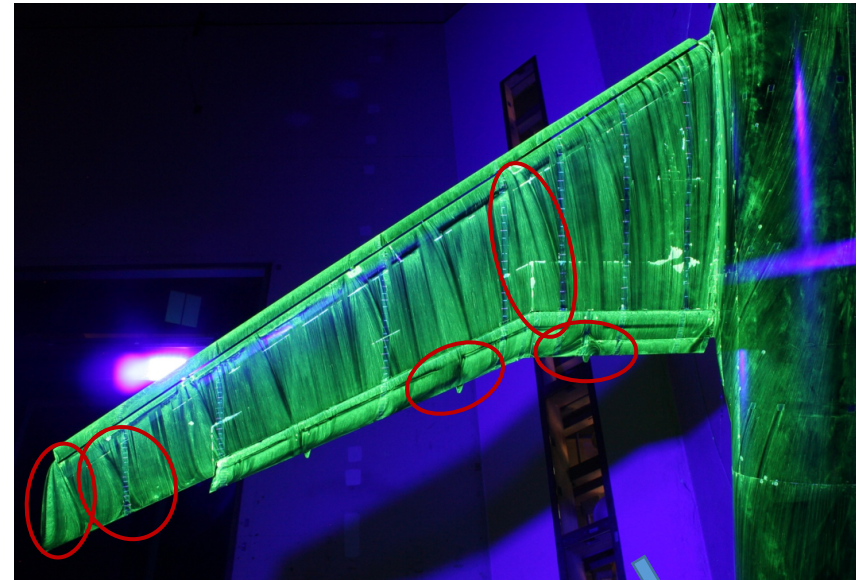
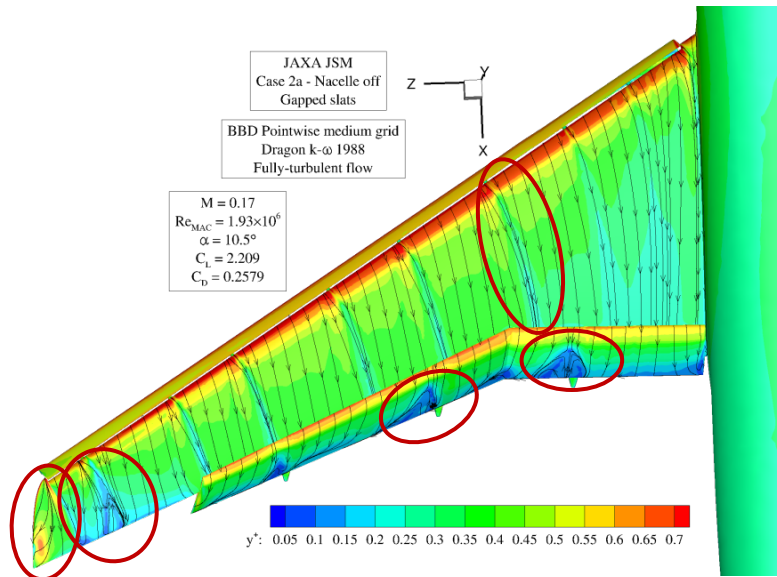


JAXA JSM results – Transition influence: forces & moments



JAXA JSM results

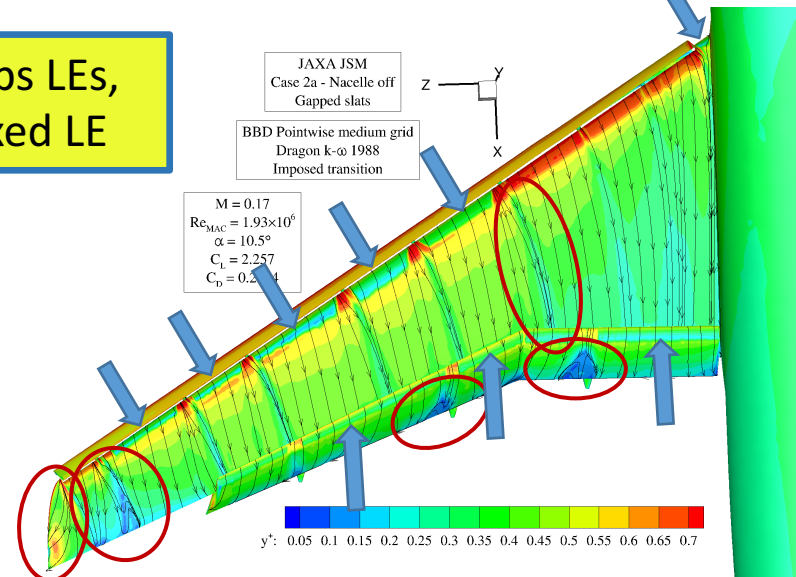
Transition influence: surface flow pattern at mid α



Laminar flow on flaps LEs,
OB WUSS and IB fixed LE

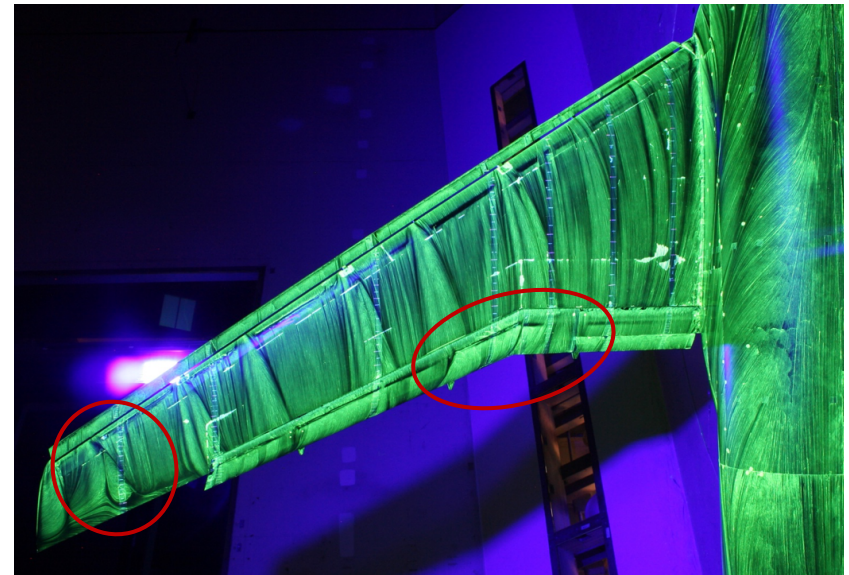
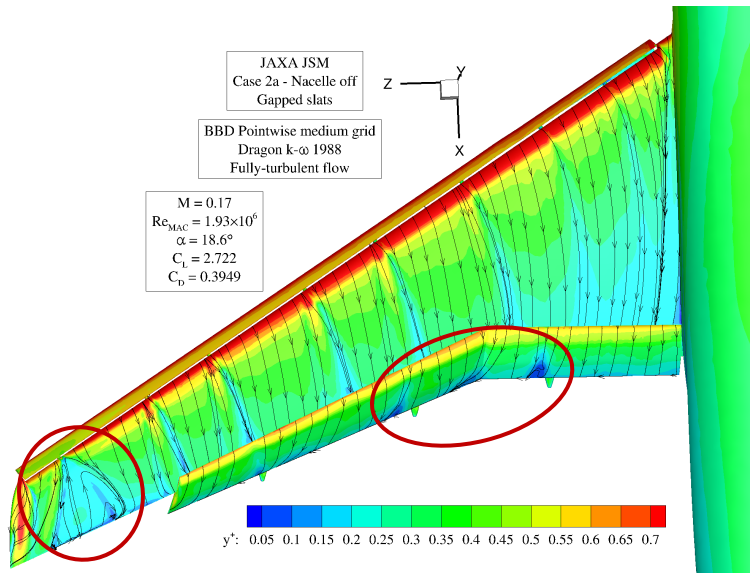
Flow pattern well predicted overall:

- Flow separation behind FTFs
- Flow separation behind most-OB slat track
 - Wingtip separation
- Slat tracks vortices (lower y^+)

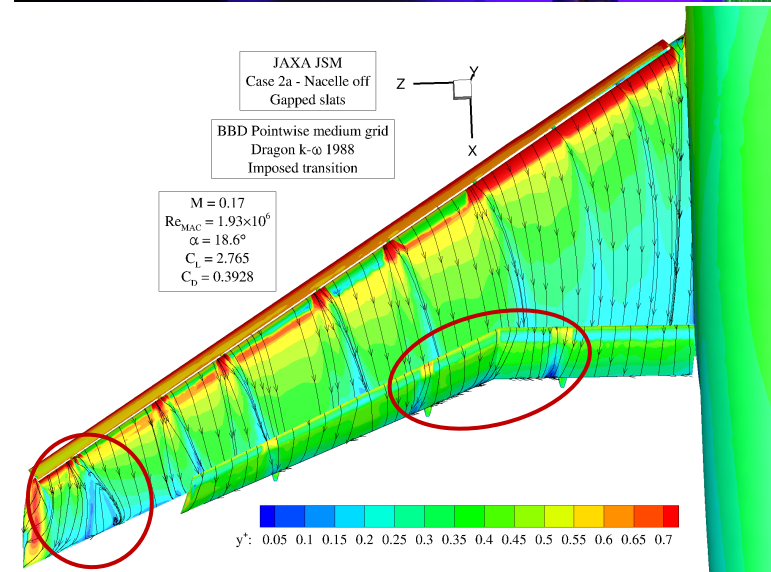


JAXA JSM results

Transition influence: surface flow pattern at high α

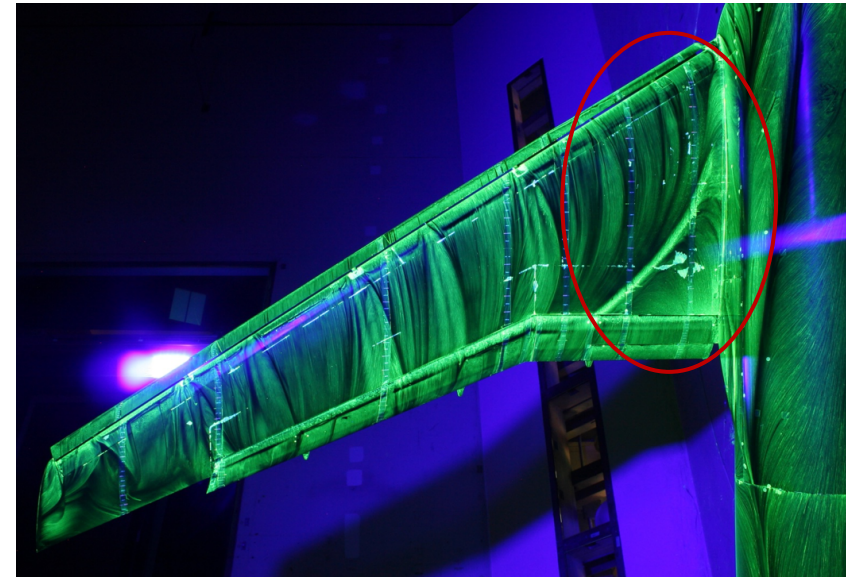
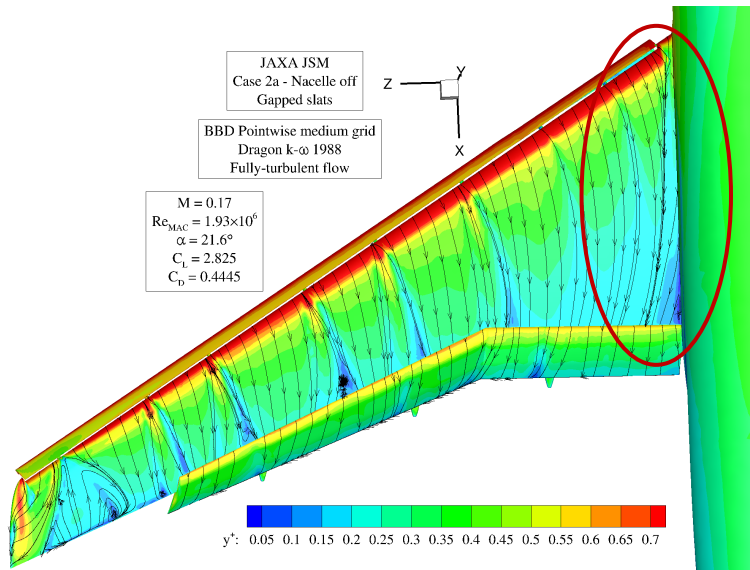


FT solution overpredicts
extent of flow separation
behind most-OB slat track
and FTFs



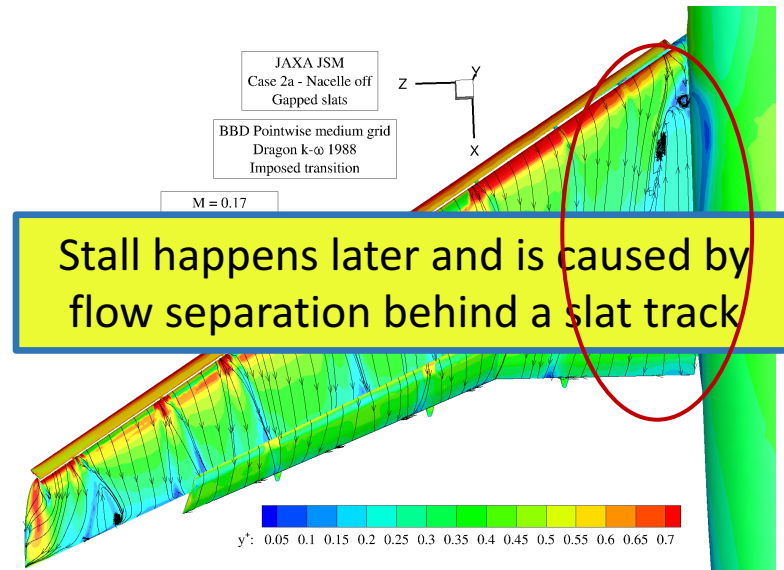
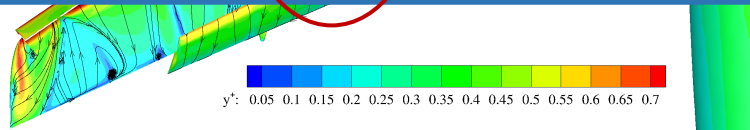
JAXA JSM results

Transition influence: surface flow pattern post-stall



FT solution does not predict IB separation

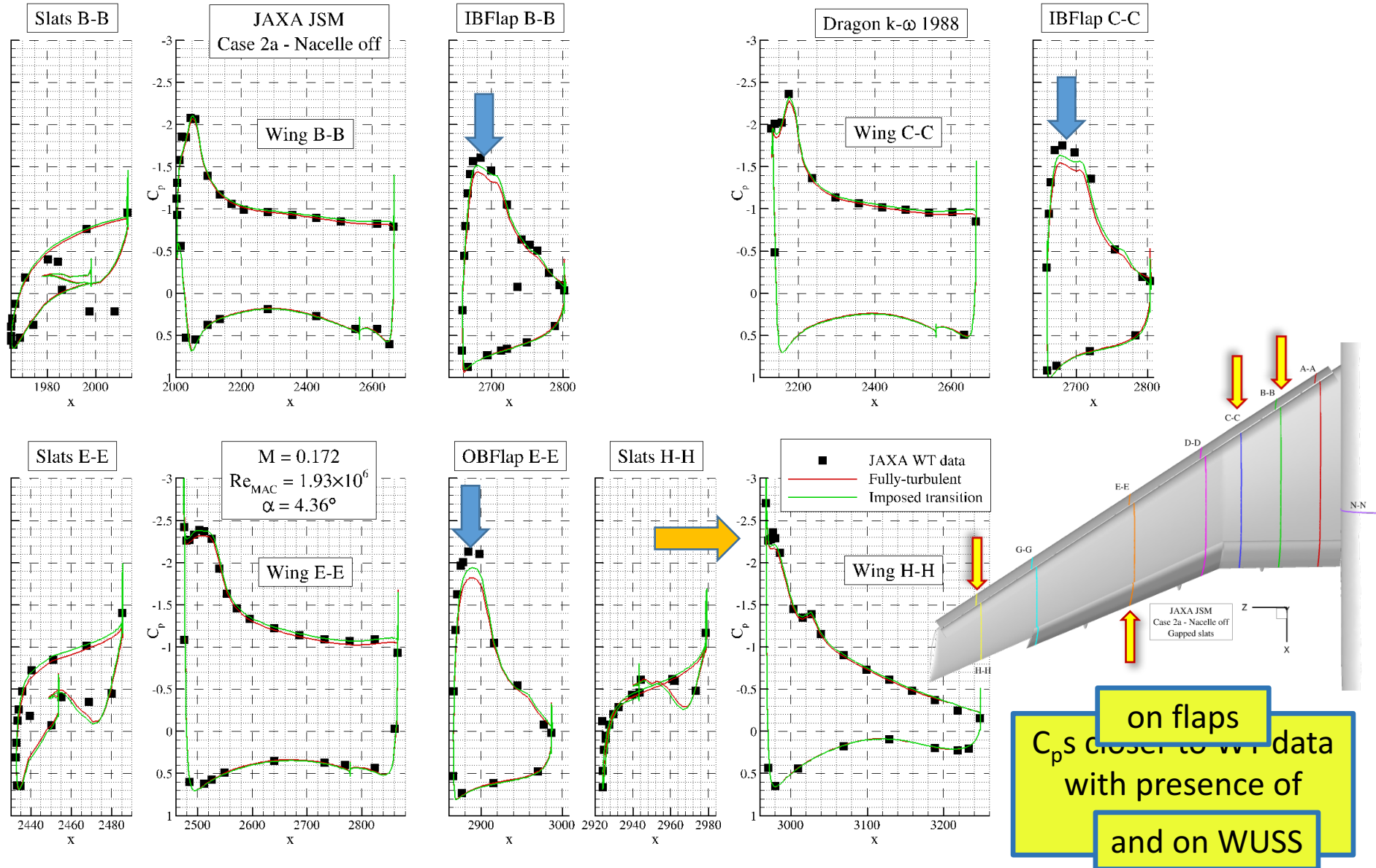
Prediction improved with laminar flow on fixed IB LE



Stall happens later and is caused by flow separation behind a slat track

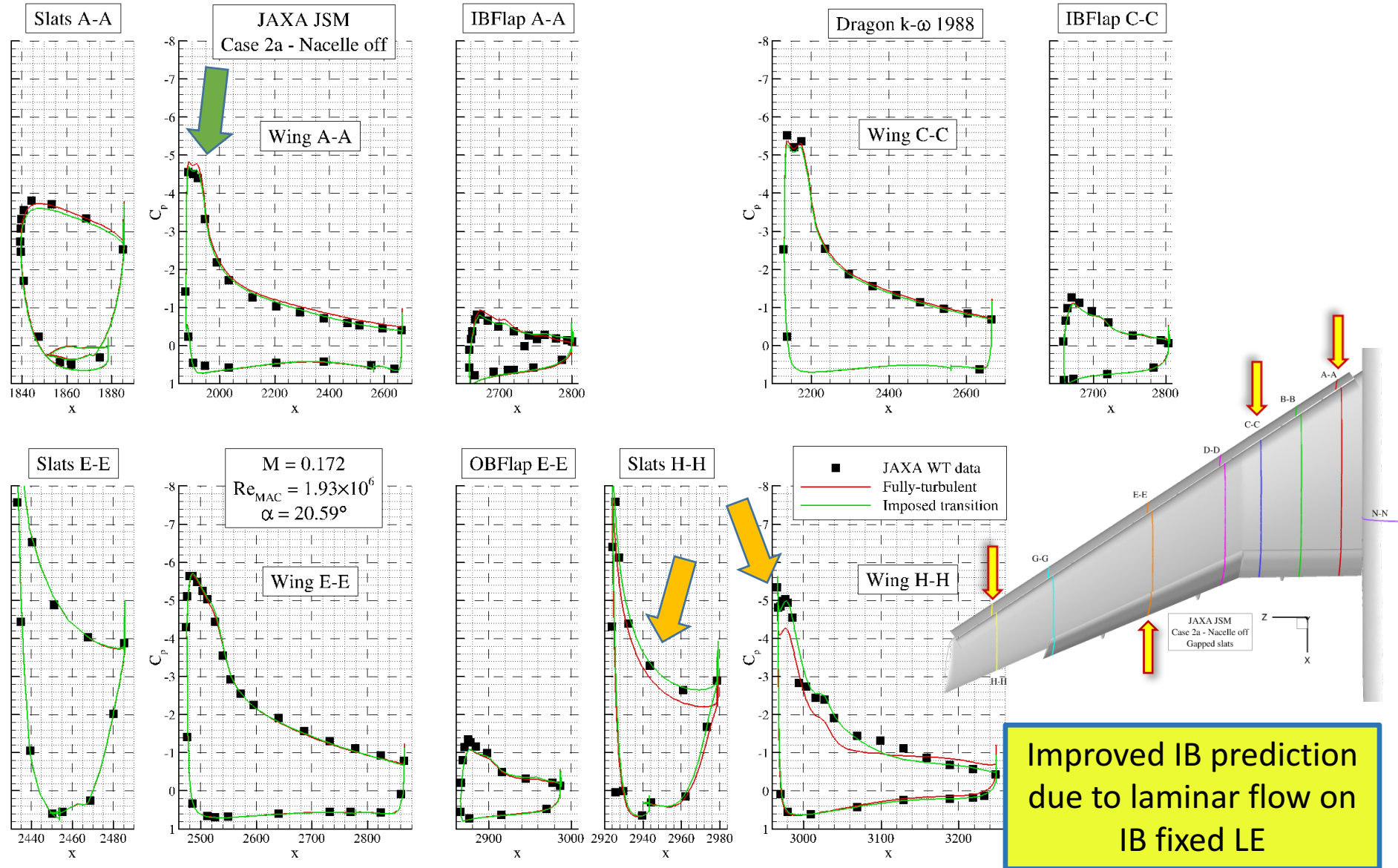
JAXA JSM results

Transition influence: pressure distributions at low α



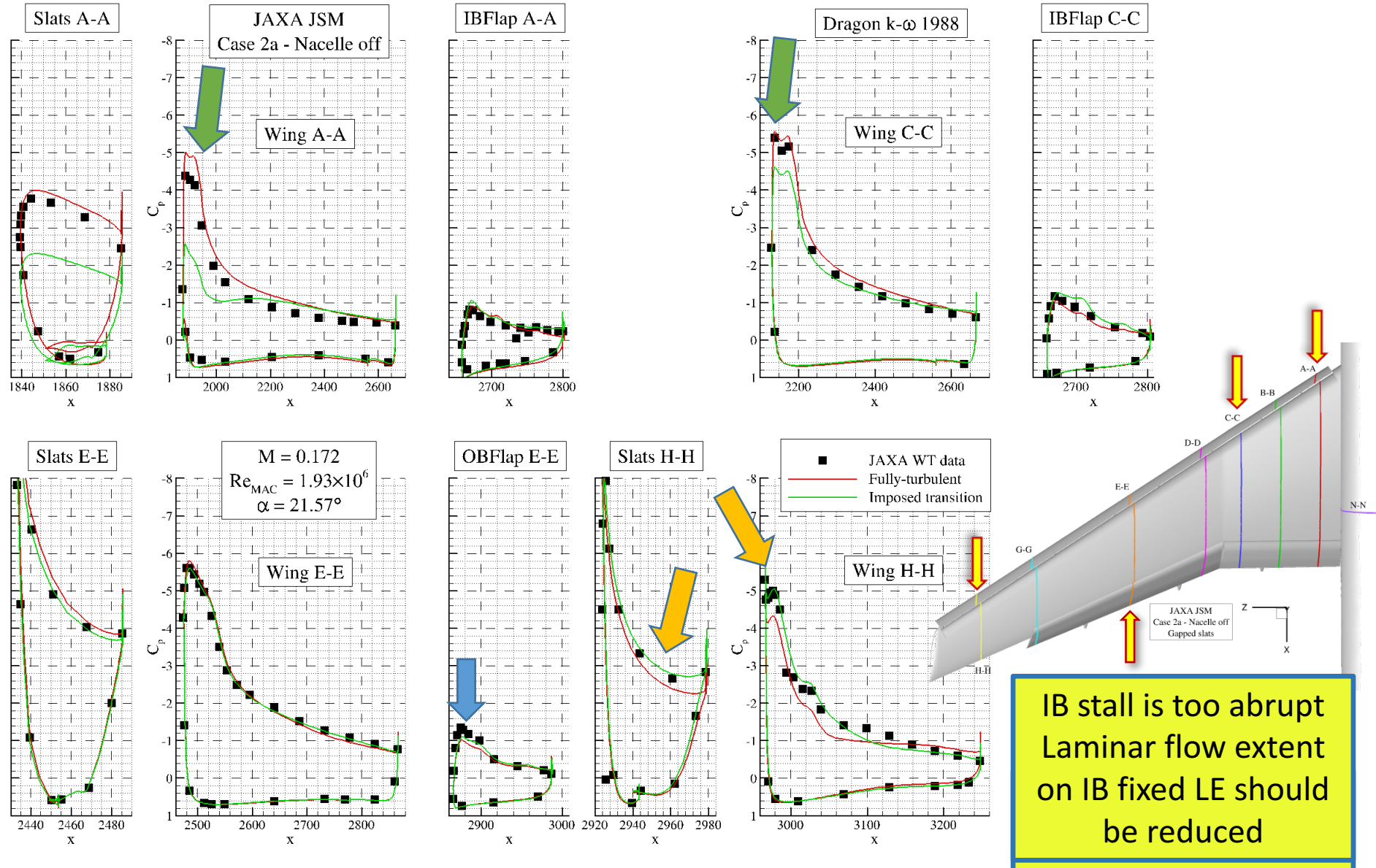
JAXA JSM results

Transition influence: pressure distributions at stall



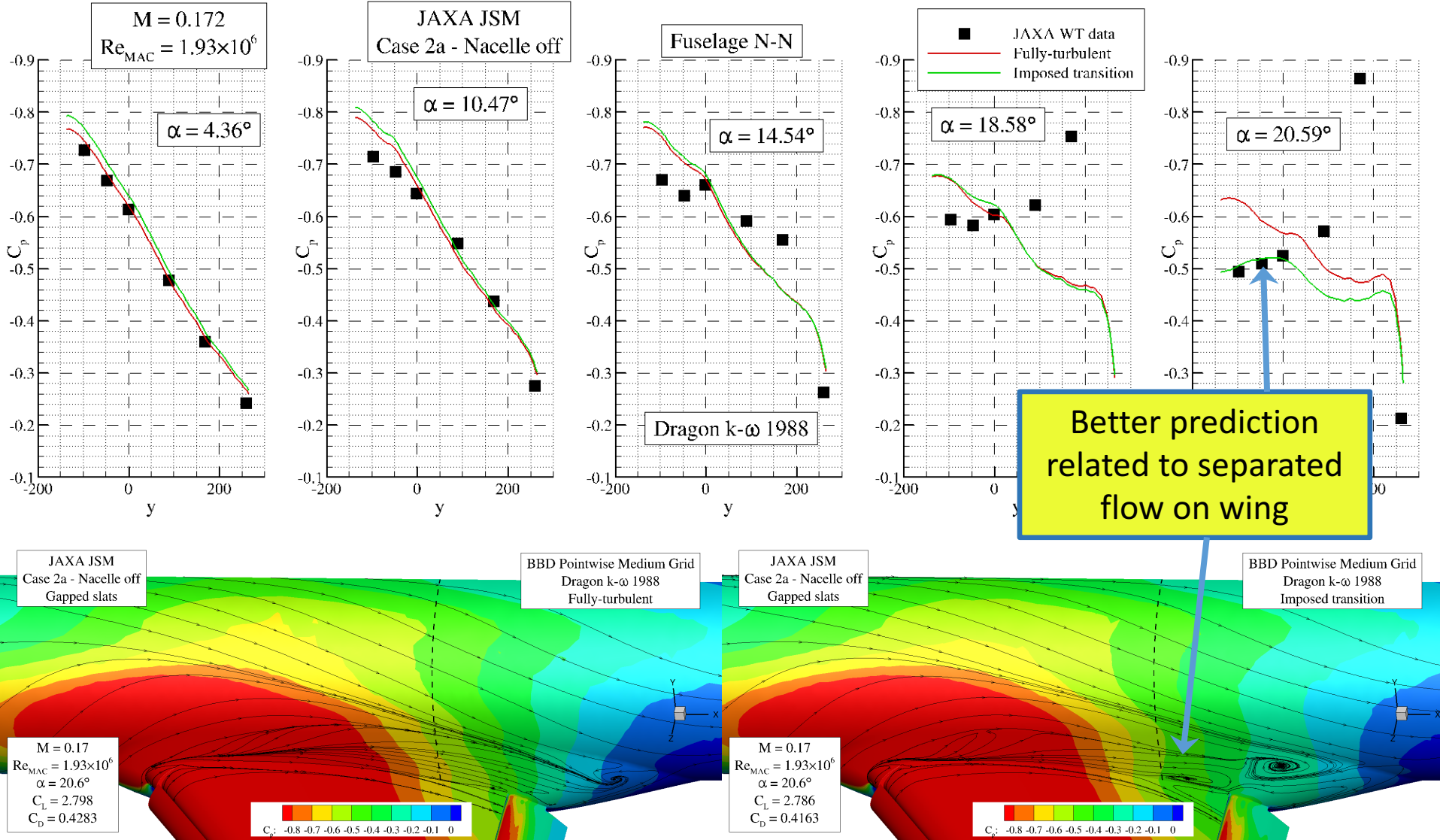
JAXA JSM results

Transition influence: pressure distributions post-stall



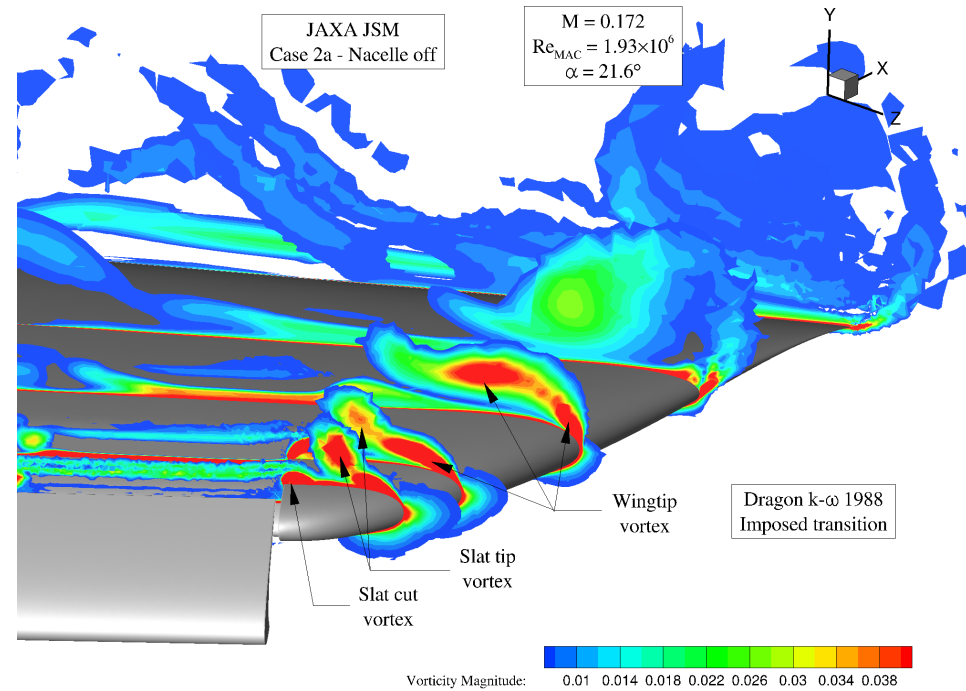
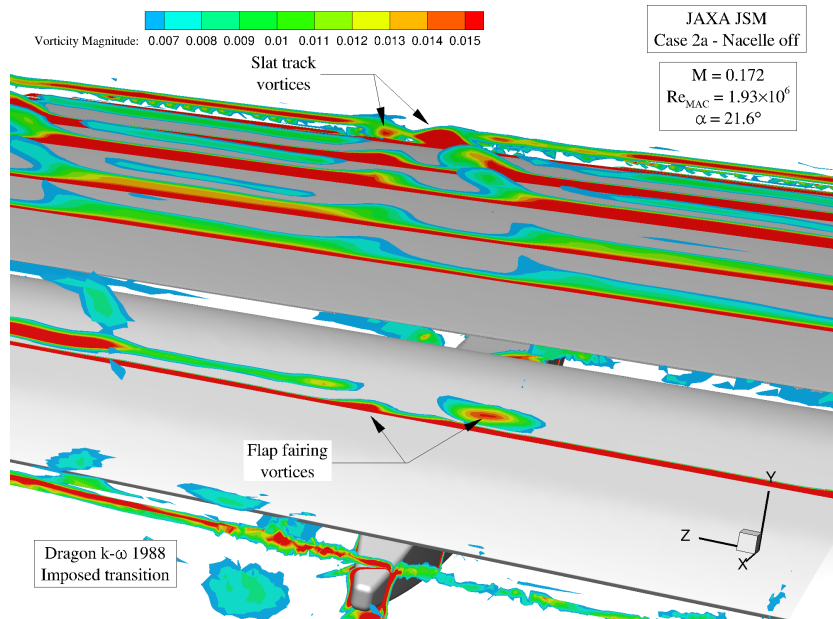
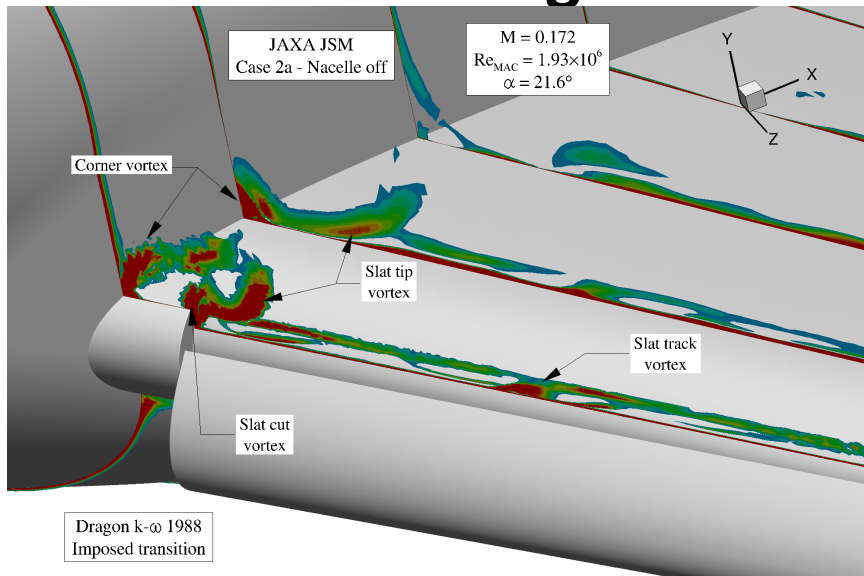
JAXA JSM results

Transition influence: pressure distributions



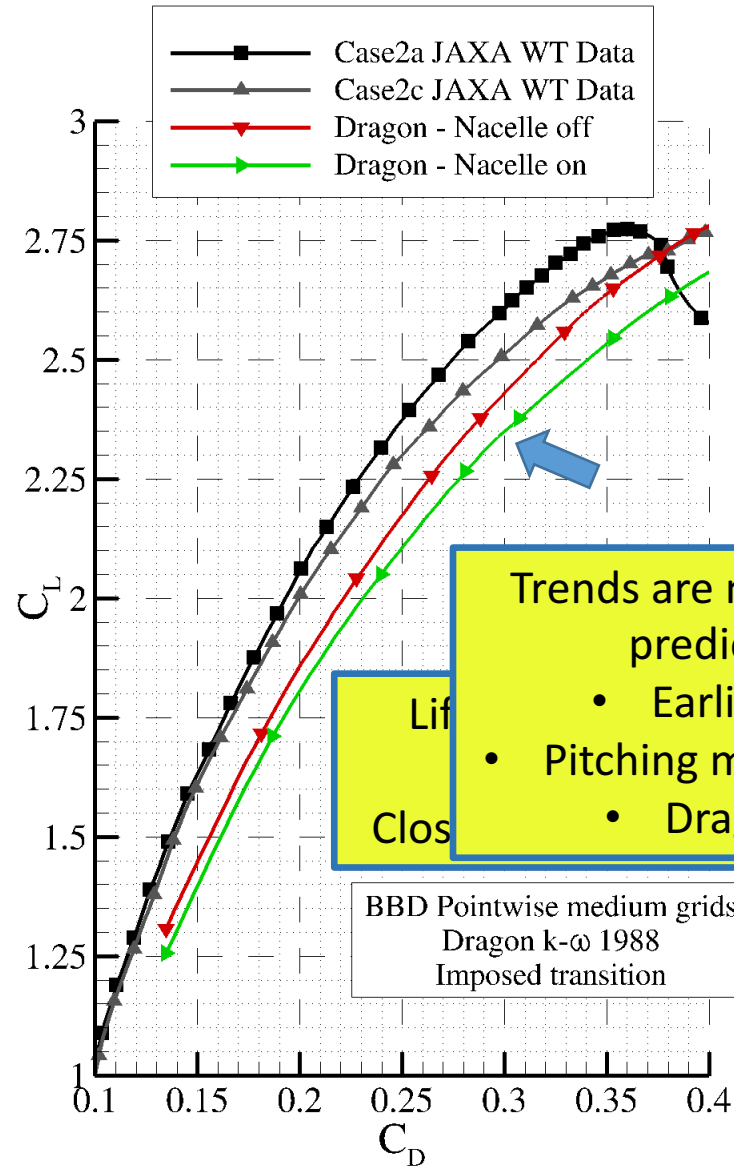
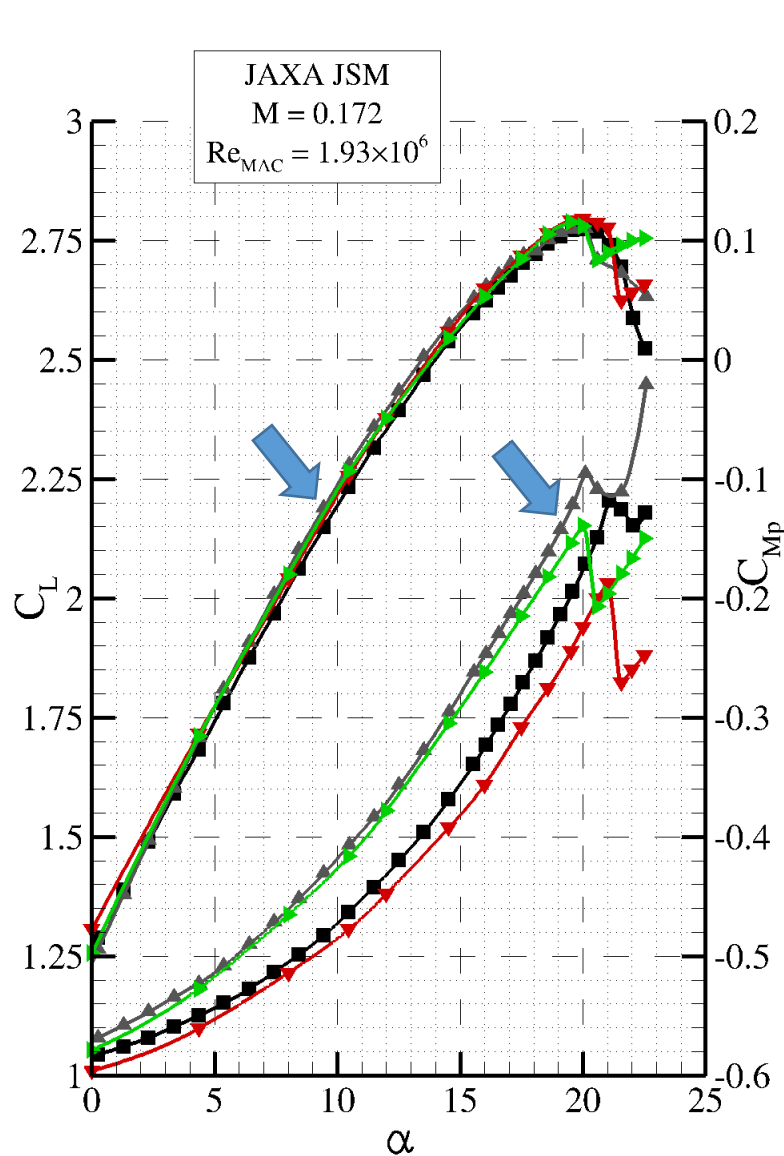
JAXA JSM results

Nacelle-off configuration: volume plots (post-stall)

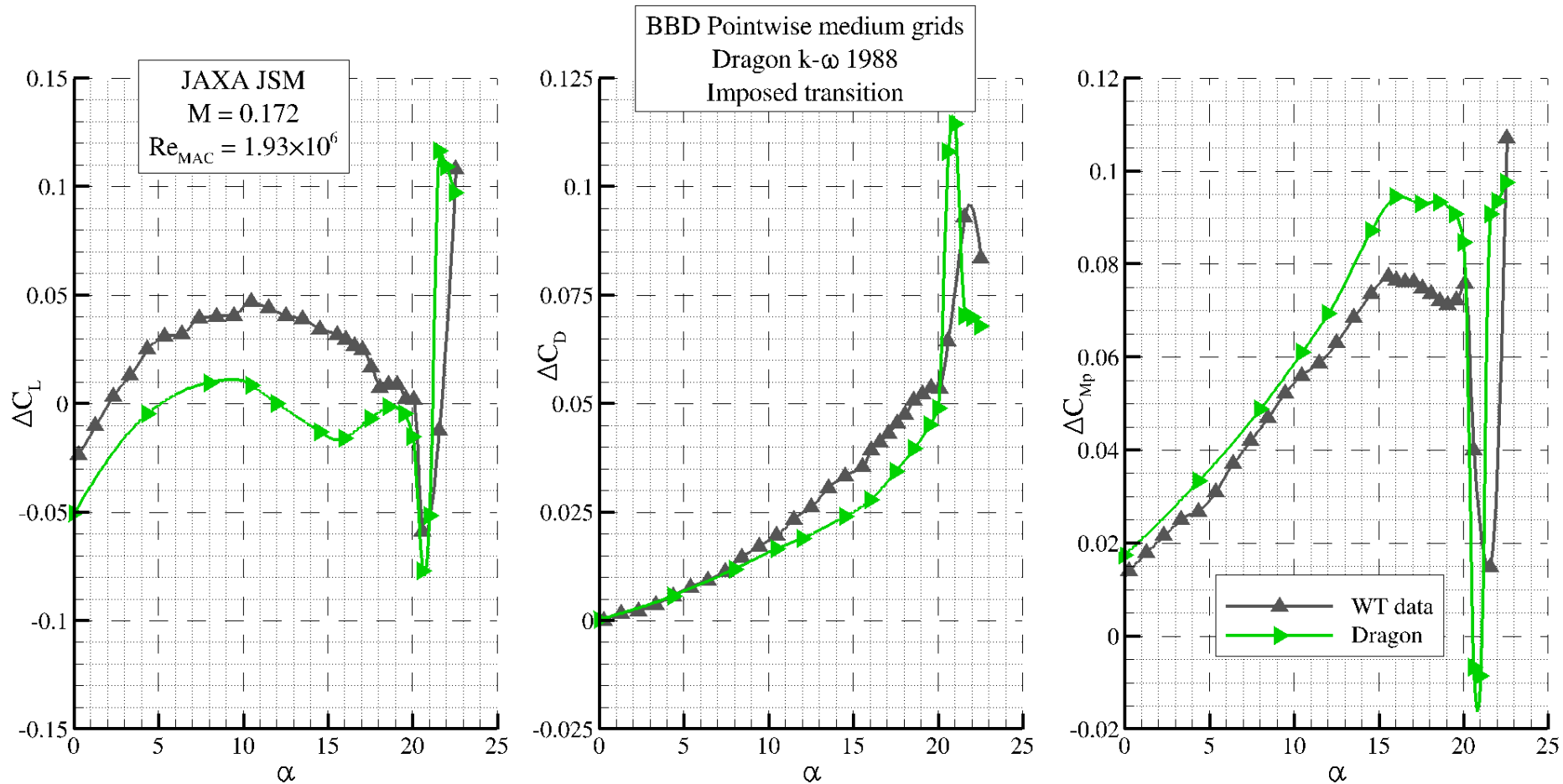


Main flow features are captured
but likely dissipate too quickly
Volumic refinement/adaptation
would be required

JAXA JSM results – Nacelle installation: forces & moments

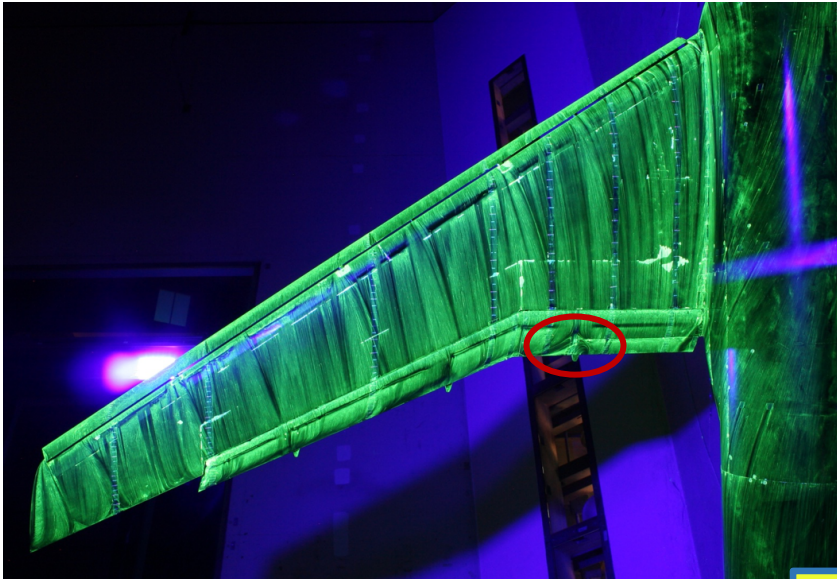


JAXA JSM results – Nacelle installation: forces & moments



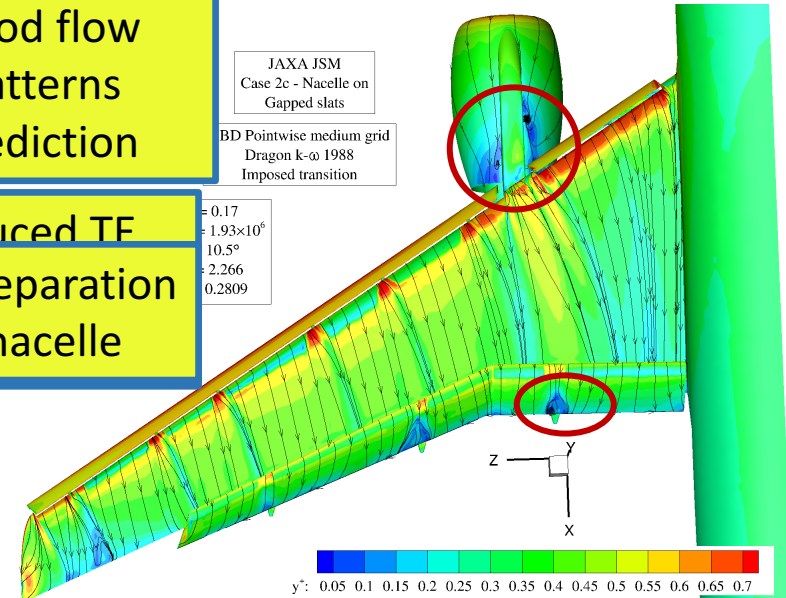
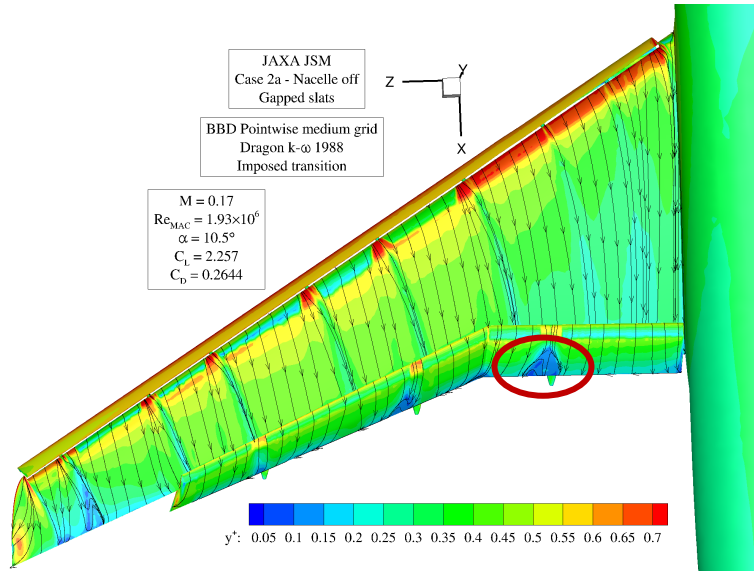
JAXA JSM results

Nacelle installation: surface flow pattern (mid α)



Good flow
patterns
prediction

Reduced TF
Flow separation
on nacelle

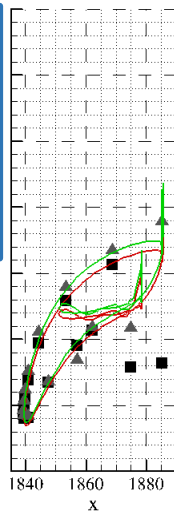


JAXA JSM results

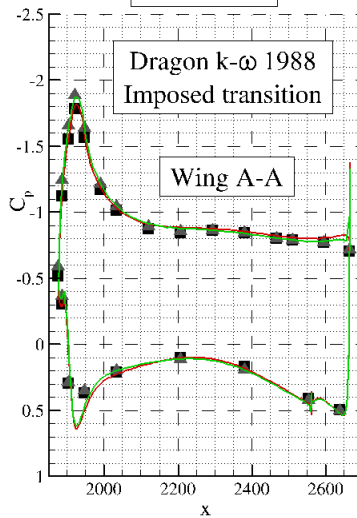
Nacelle installation: pressure distributions at low α

Impact of nacelle on C_p s is well predicted

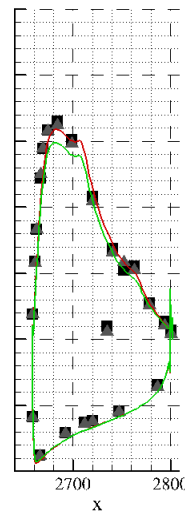
Slats A-A



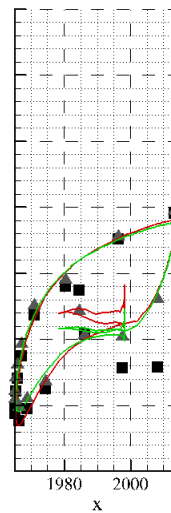
JAXA JSM



IBFlap A-A

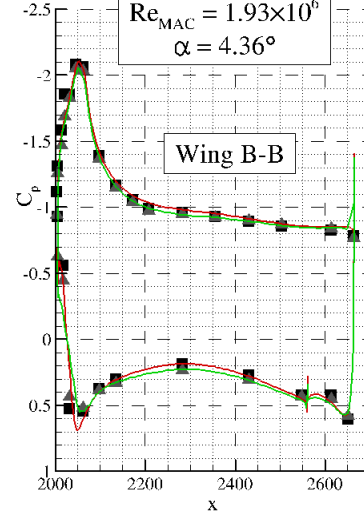


Slats B-B

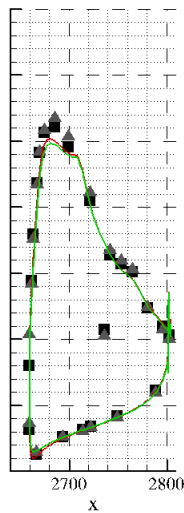


$M = 0.172$
 $Re_{MAC} = 1.93 \times 10^6$
 $\alpha = 4.36^\circ$

Wing B-B

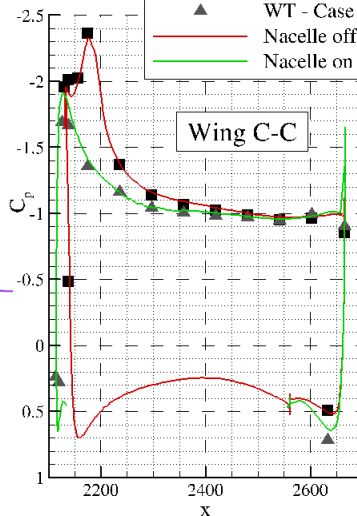


IBFlap B-B

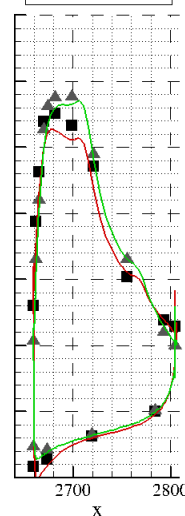


■ WT - Case 2a
▲ WT - Case 2c
— Nacelle off
— Nacelle on

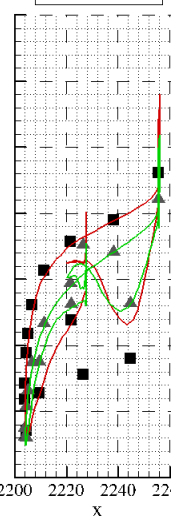
Wing C-C



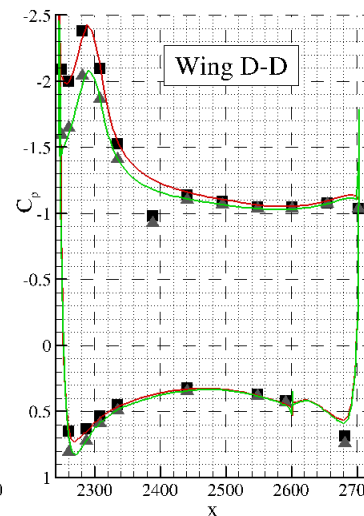
IBFlap C-C



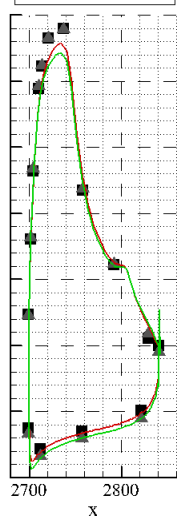
Slats D-D



Wing D-D

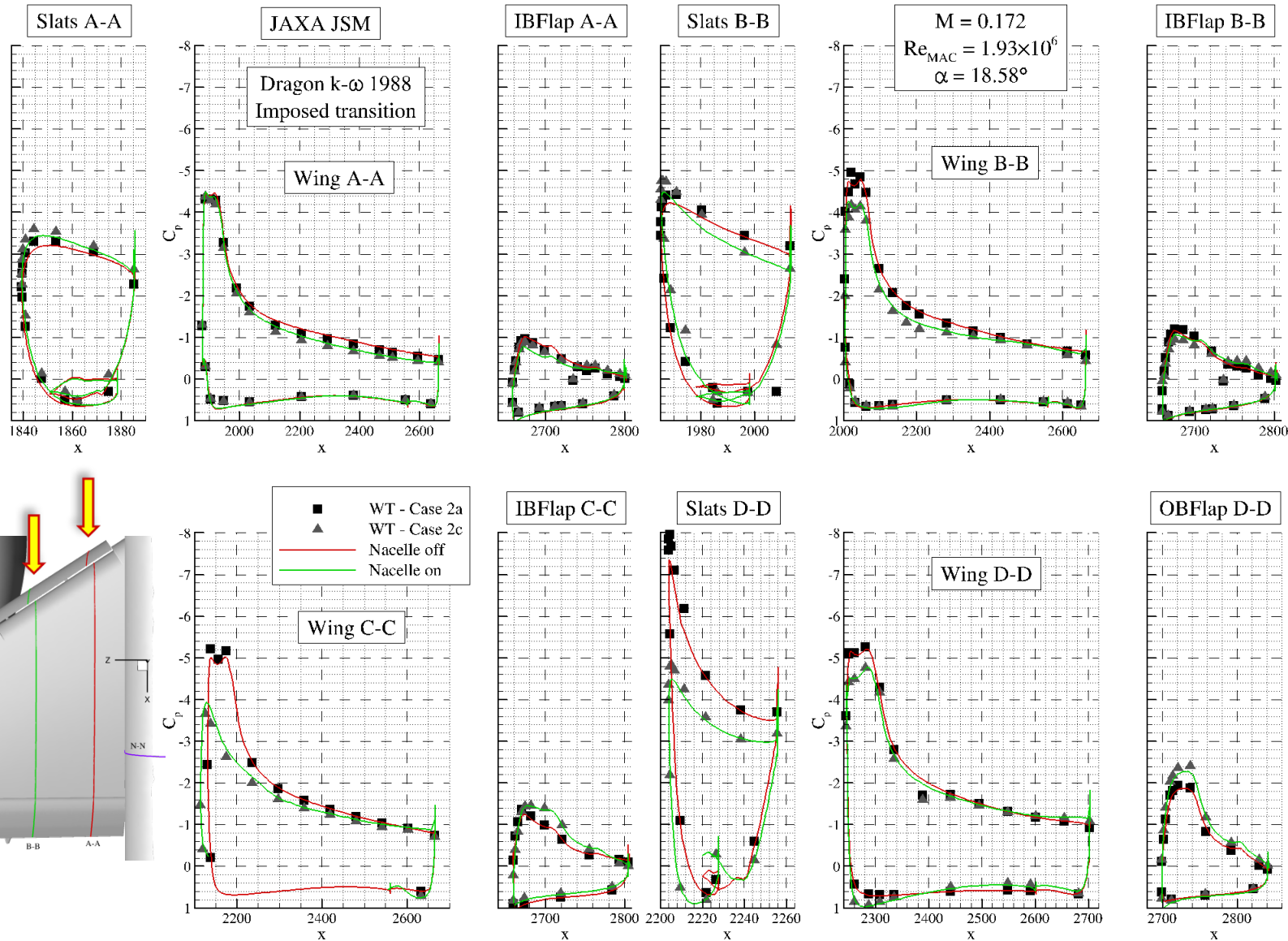


OBFlap D-D



JAXA JSM results

Nacelle installation: pressure distributions at high α



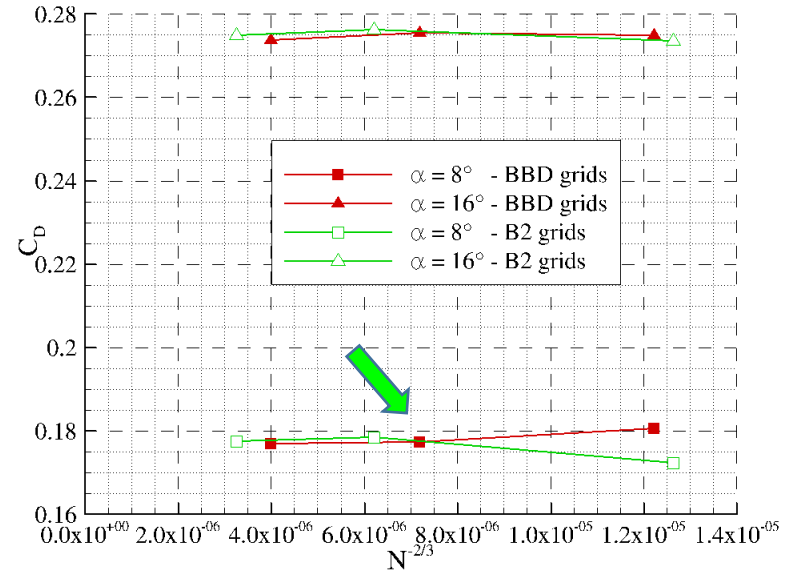
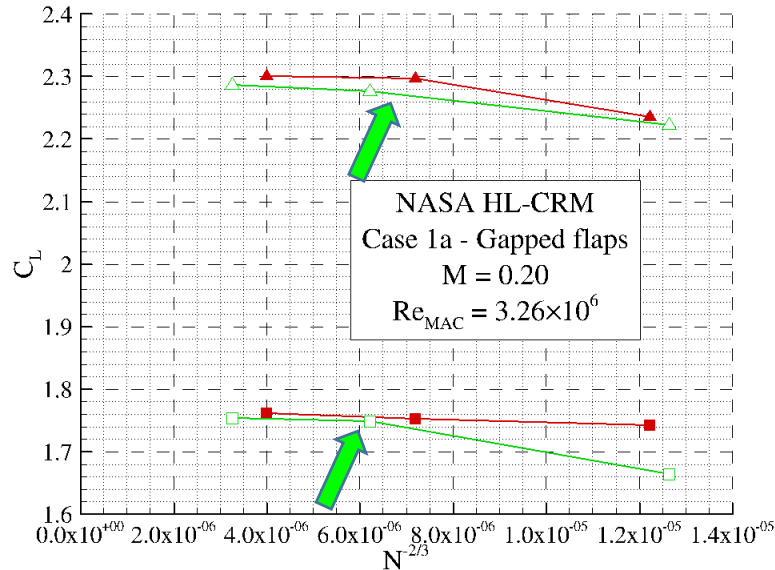
NASA CRM grid systems

Bombardier Pointwise grids		Case 1a Coarse Grid	Case 1a Medium Grid	Case 1a Fine Grid	Case 1c Coarse Grid	Case 1c Medium Grid
Number of nodes		9 482 482				
Number of cells		23 379 645				
Committee B2 (Pointwise) grids		Case 1a Coarse Grid	Case 1a Medium Grid	Case 1a Fine Grid		
Number of nodes		8 084 687	26 499 283	69 909 799		
Number of cells		22 250 370	64 628 961	238 935 944		
# of surface elements	BBD Coarse	B2 Coarse	BBD Medium	B2 Medium	BBD Fine	B2 Fine
Fuselage	23 401	73 441	38 738	183 098	63 140	407 763
Wing	205 767	219 140	109 564	109 278	237 172	139 828
Slats	129 410	126 040				
IB flap	53 028	14 420				
OB flap	67 256	19 858				

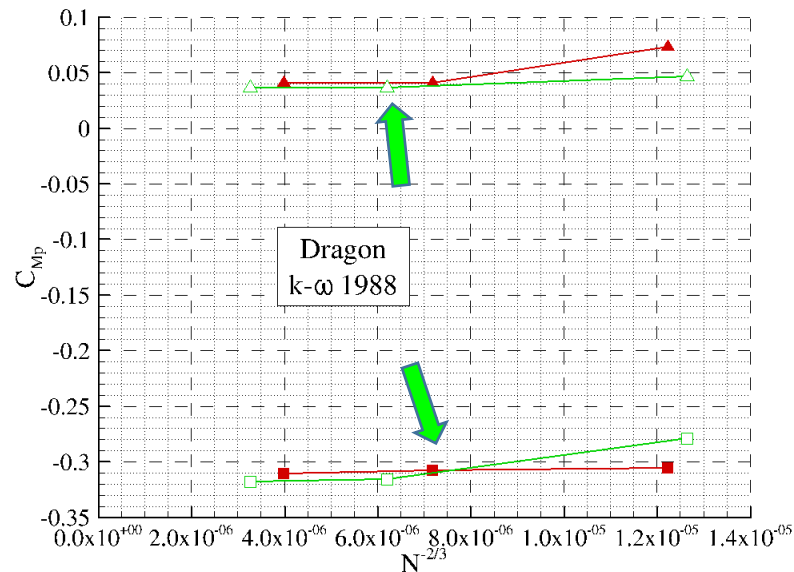
But B2 coarse grid has 3 times as many elements on the fuselage and less of a third on the flaps
The B2 fine grid has as many elements on the slats as on the wing

Bombardier and B2 coarse and medium grids have similar number of nodes and cells
B2 fine grid has almost twice as many cells as Bombardier fine grid

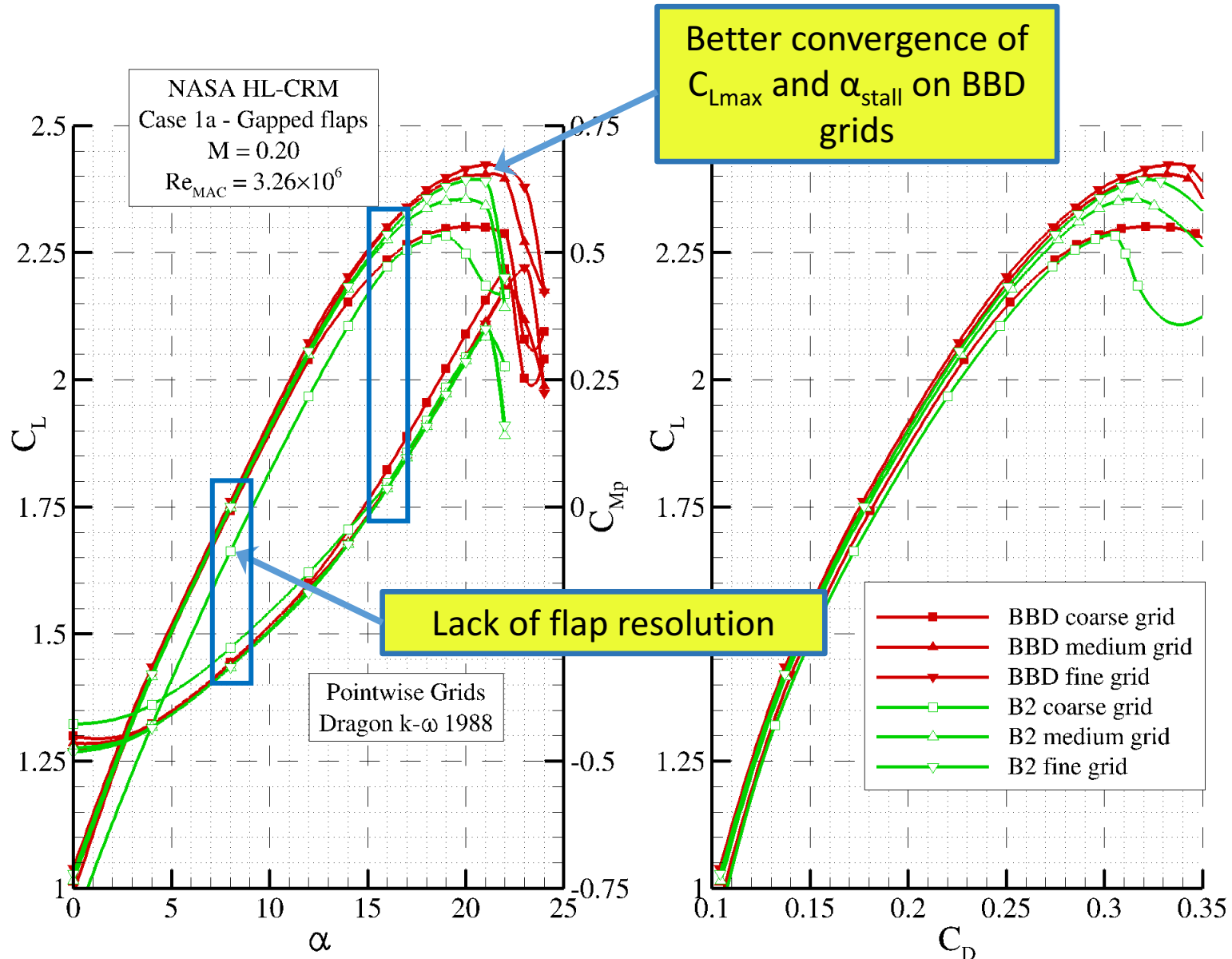
HL-CRM results – Grid convergence



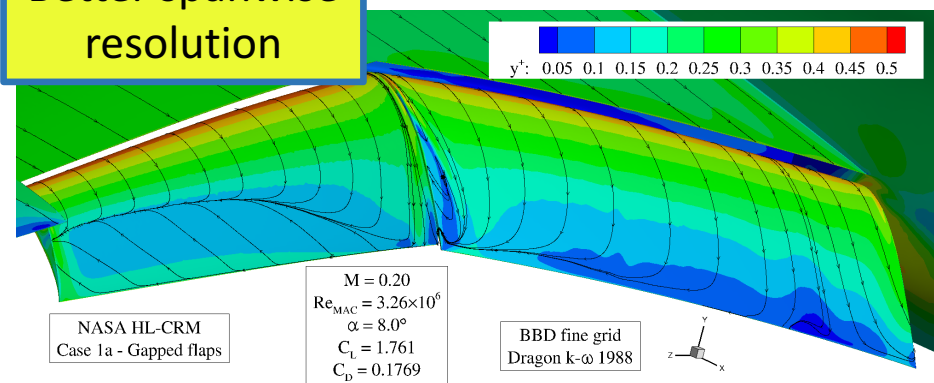
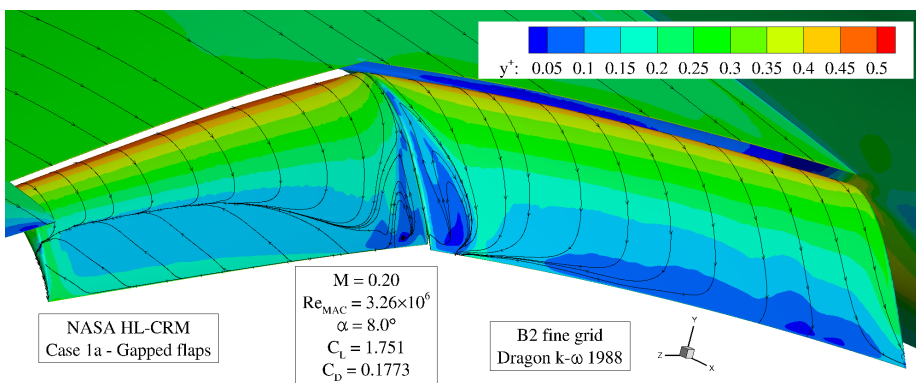
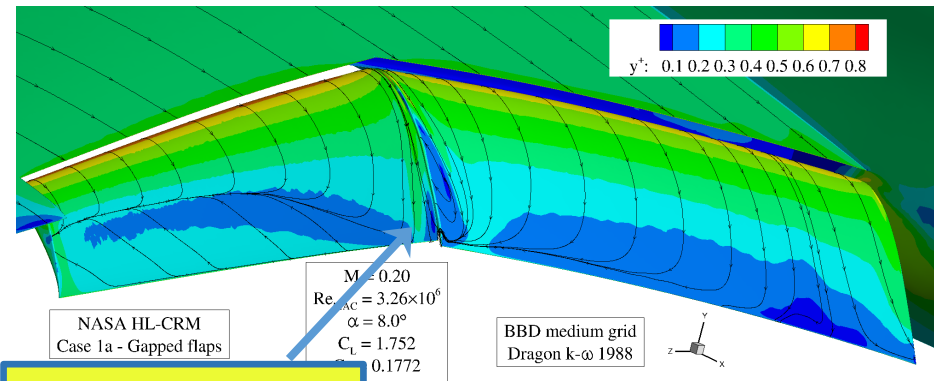
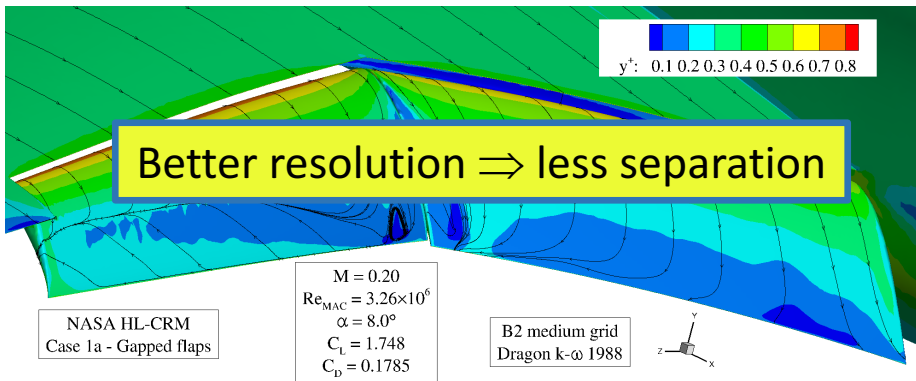
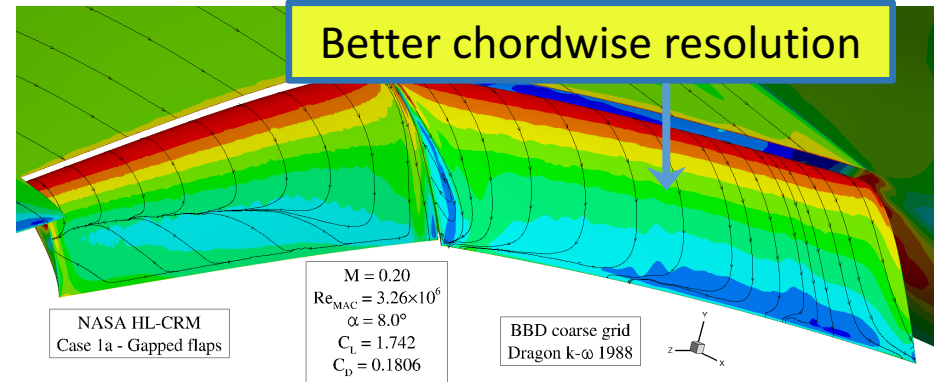
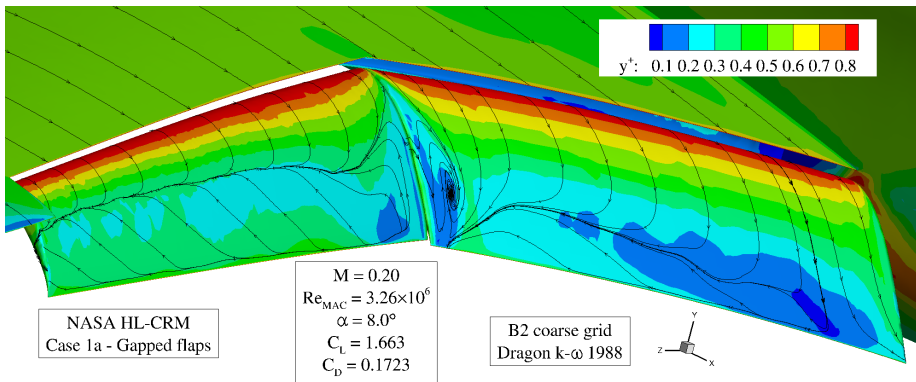
Grid convergence
achieved on
medium grids



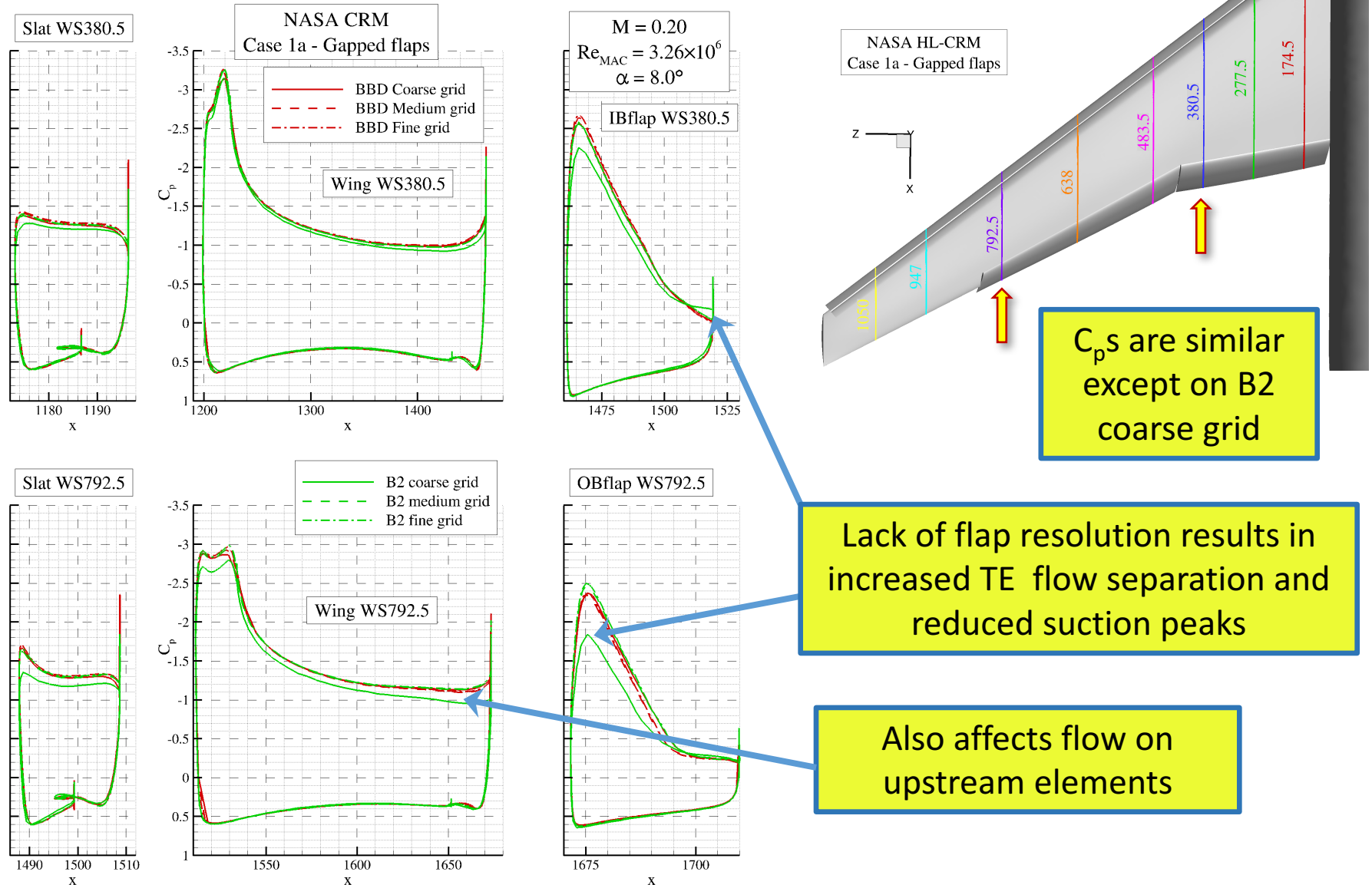
HL-CRM results – Grid influence: forces and moments



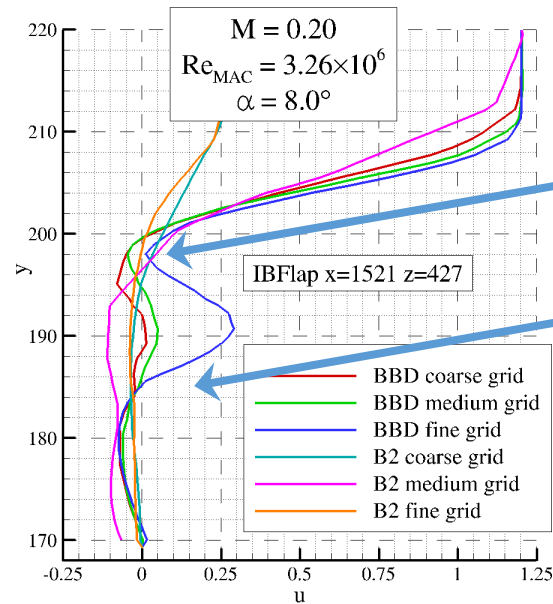
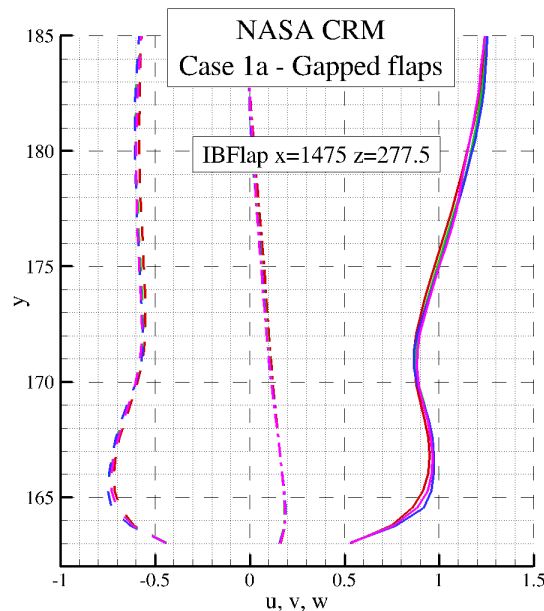
HL-CRM results – Grid influence: flaps flow pattern



HL-CRM results – Grid influence: pressure distribution



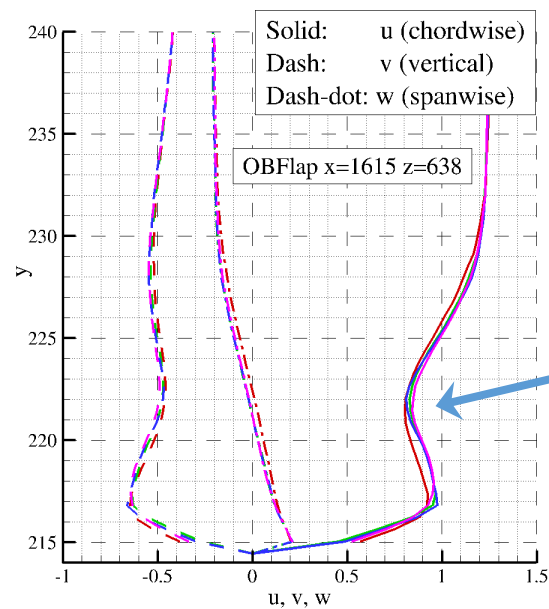
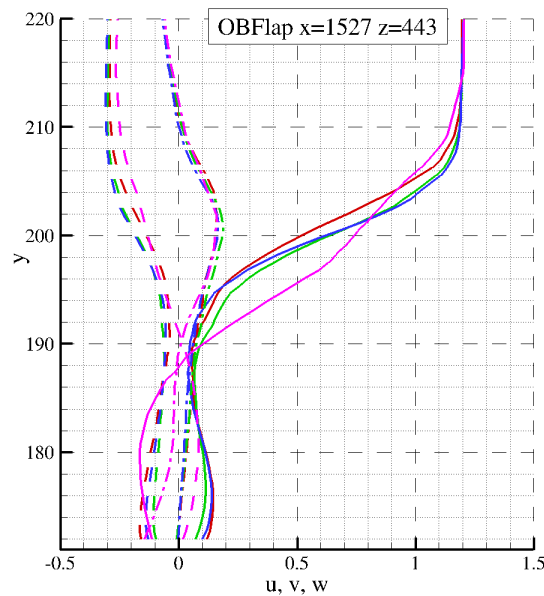
HL-CRM results – Grid influence: velocity profiles



Wing wake

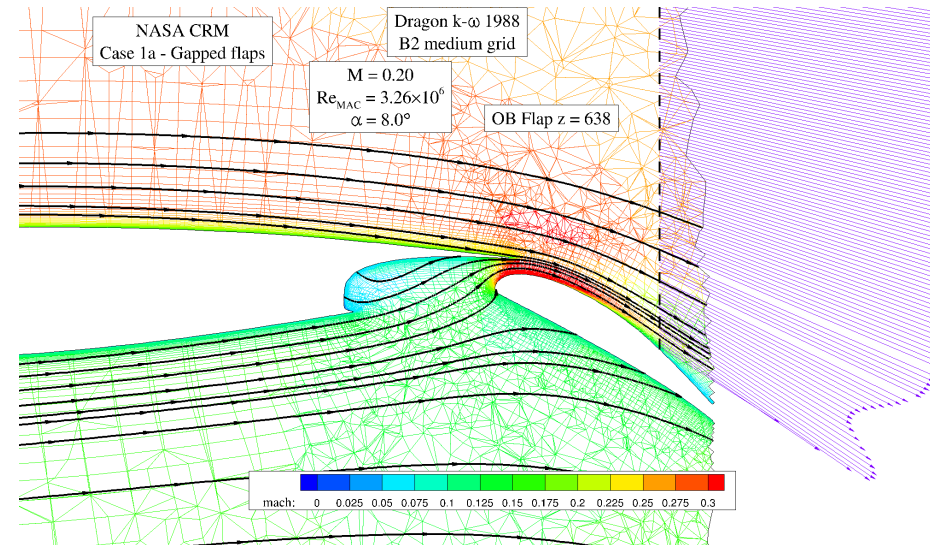
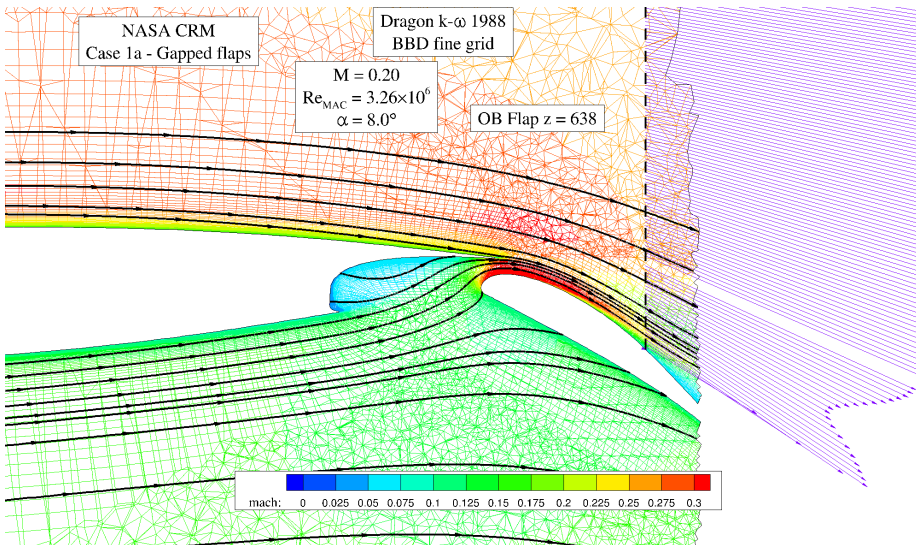
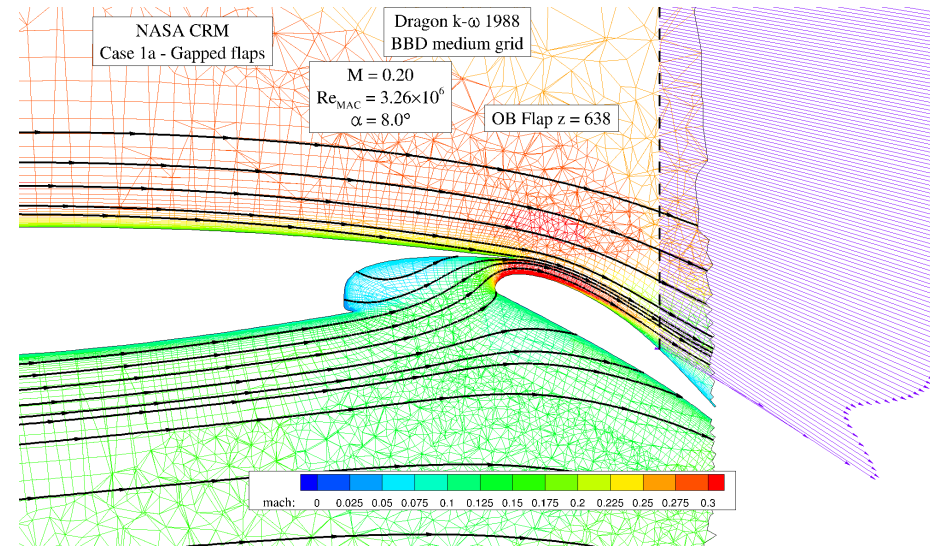
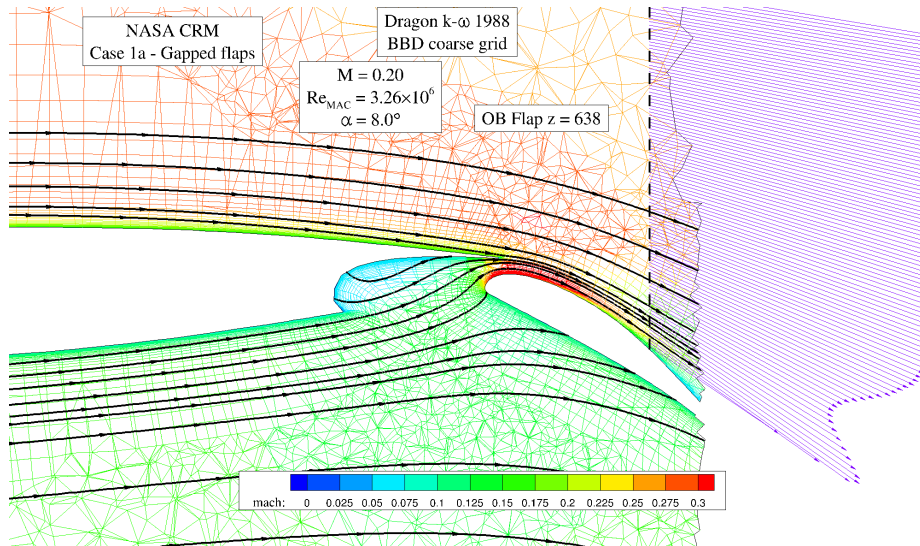
Separated flow

Good agreement among solutions for attached flow
More significant variations in separated flow areas

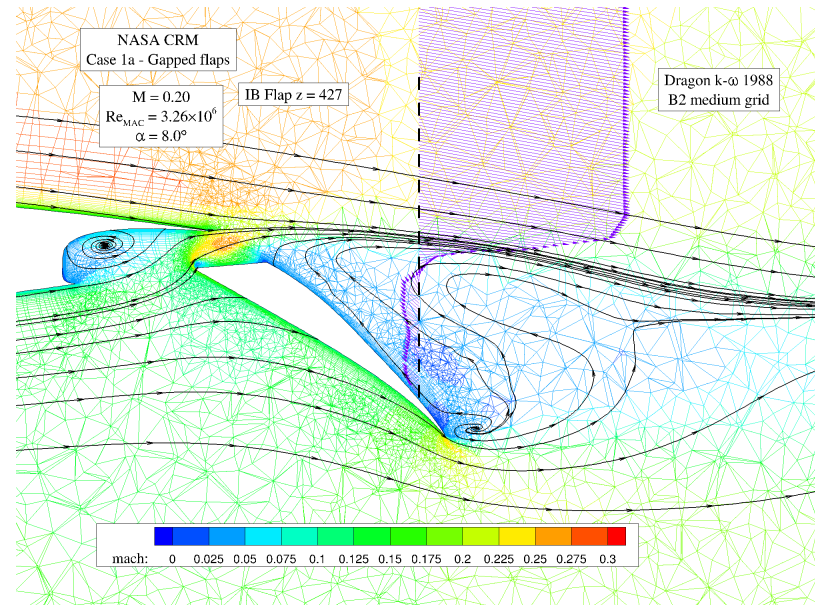
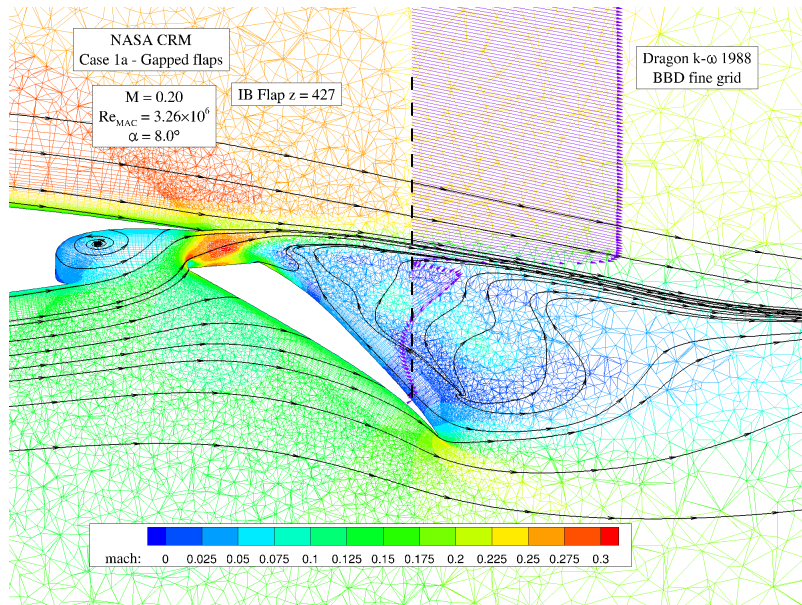
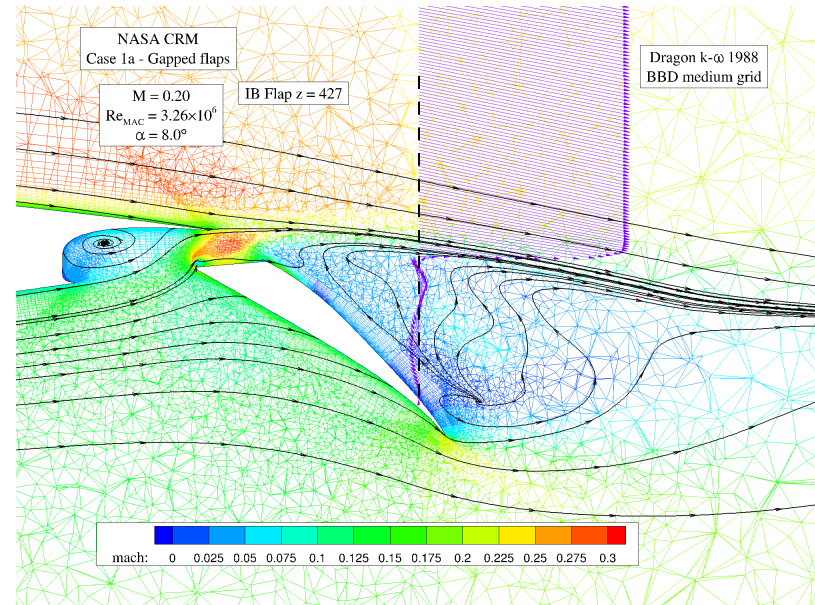
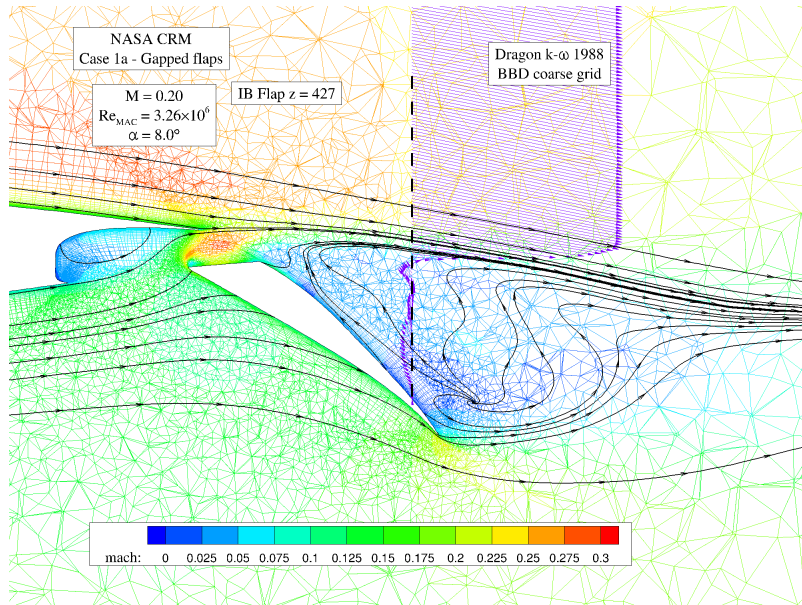


Wing wake

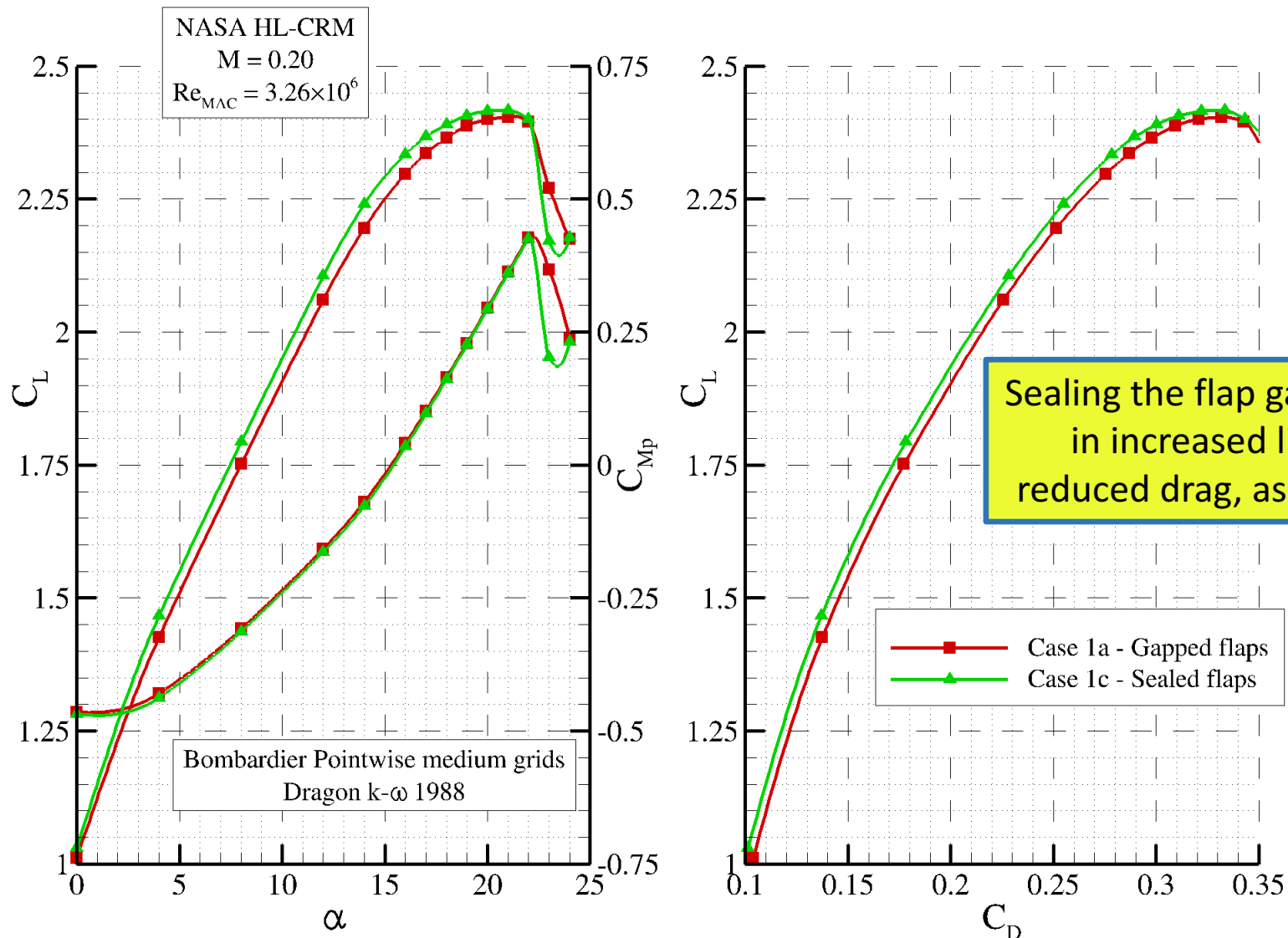
HL-CRM results – Grid influence: velocity profiles



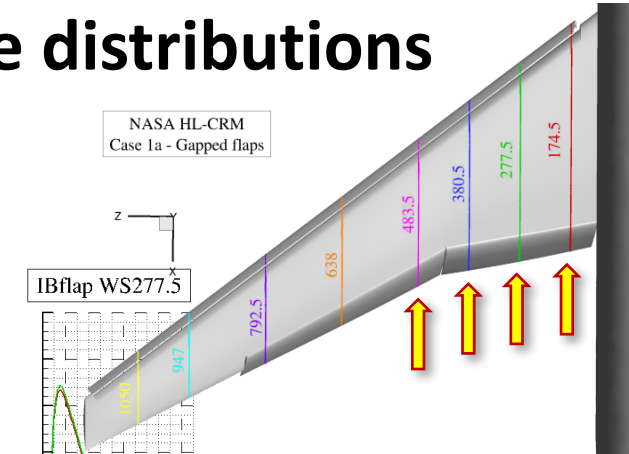
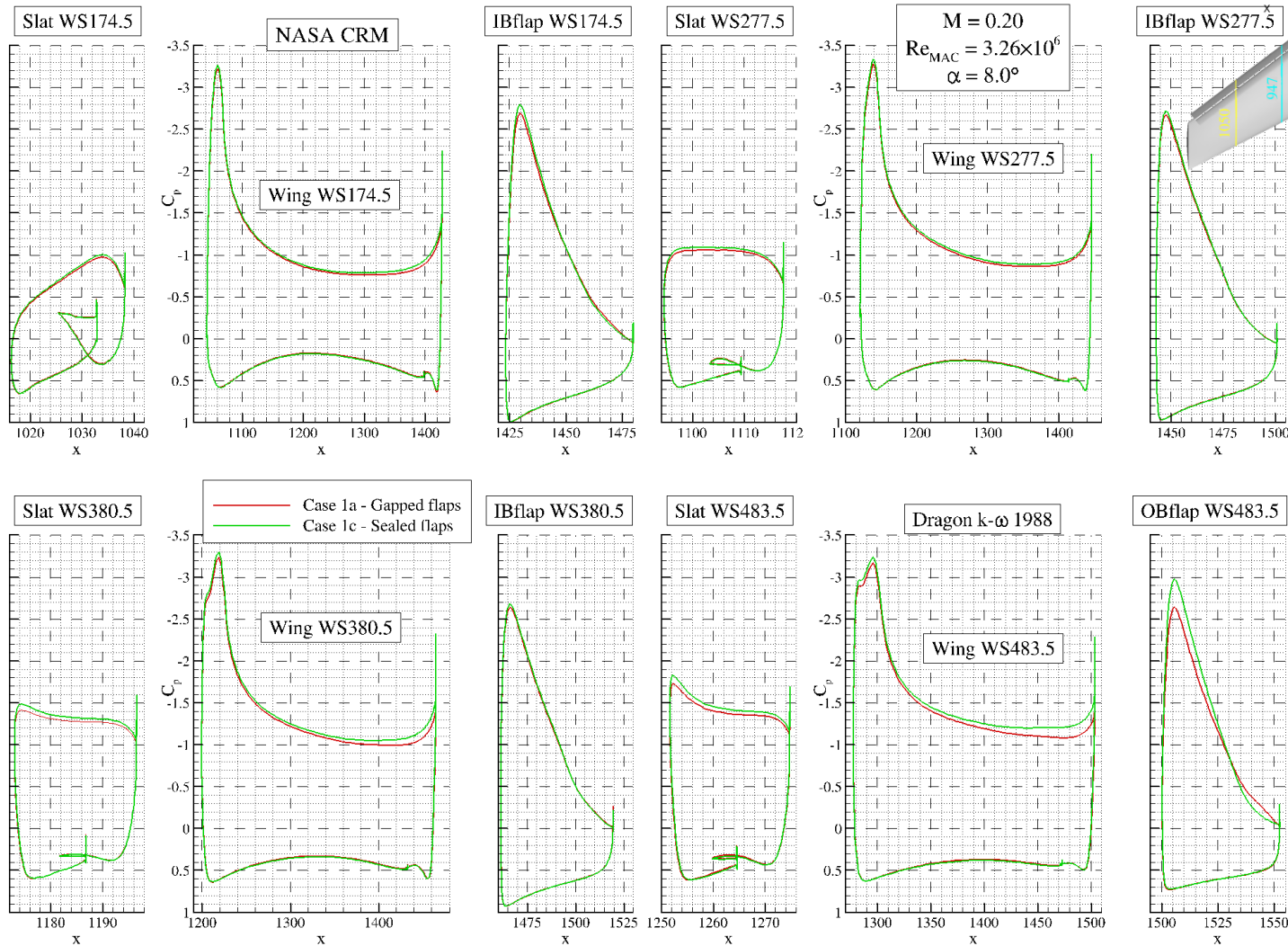
HL-CRM results – Grid influence: velocity profiles



HL-CRM results – Flaps sealing: forces and moments



HL-CRM results – Flaps sealing: pressure distributions



Influence of sealing is local: mid-flap C_p s are not affected

HL-CRM results – Flaps sealing: flaps flow pattern

NASA HL-CRM
Case 1a - Gapped flaps

$M = 0.20$
 $Re_{MAC} = 3.26 \times 10^6$
 $\alpha = 8.0^\circ$
 $C_L = 1.752$
 $C_D = 0.1772$

BBD medium grid
Dragon k- ω 1988

C_p : -2.5 -2.25 -2 -1.75 -1.5 -1.25 -1 -0.75 -0.5 -0.25 0

NASA HL-CRM
Case 1c - Sealed flaps

$C_L = 1.793$
 $C_D = 0.1780$

BBD medium grid
Dragon k- ω 1988

C_p : -2.5 -2.25 -2 -1.75 -1.5 -1.25 -1 -0.75 -0.5 -0.25 0

Sealing the inter-flap gap removes a tip vortex that caused the flow to separate on the IB flap and reattach on the OB flap. Overall, more attached flow and increased C_p s.

Summary

- Cases 1a/1c – NASA CRM
 - Grid convergence achieved on medium grid level
 - Bombardier coarse grid with same number of nodes/cells as B2 grid provides better flow resolution
 - Surface resolution matters
 - Important to capture tip vortices
- Cases 2a/2c – JAXA JSM
 - Fully-turbulent flow assumption not valid at this low Reynolds number
 - Good prediction of lift and stall achieved with imposed transition
 - Transition prediction essential to accurately predict high-lift flows
 - Nacelle installation effects properly predicted
 - Main flow features can be captured with a medium grid but volumic refinement/adaptation could help
 - Free-stream CFD can predict half-model WT data, but discrepancies in absolute levels of drag and pitching moment can be related to half-model effect